A photograph of a wind turbine in a grassy field under a clear blue sky. The turbine is white and stands tall in the background. In the foreground, there is a wooden walkway with a railing leading towards the turbine. The field is green and lush, and there are some trees in the distance.

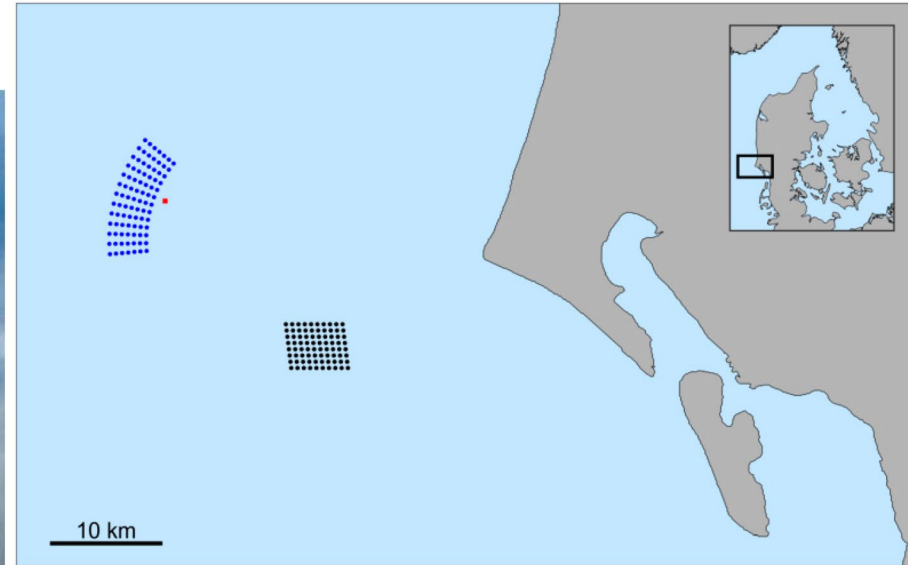
# Modeling (and observations) of wind turbine wakes

**Cristina L. Archer**  
**Center for Research in Wind (CReW), Director**  
**Geography and Spatial Sciences, Professor**  
**Mechanical Engineering, Professor**  
**University of Delaware**

National Academies – Ocean Studies Board – Washington DC, 6/1/2023  
Hydrodynamics modeling and implications for offshore wind development

# Wakes are nearly impossible to see

Horns Rev 1 (2/12/2008)

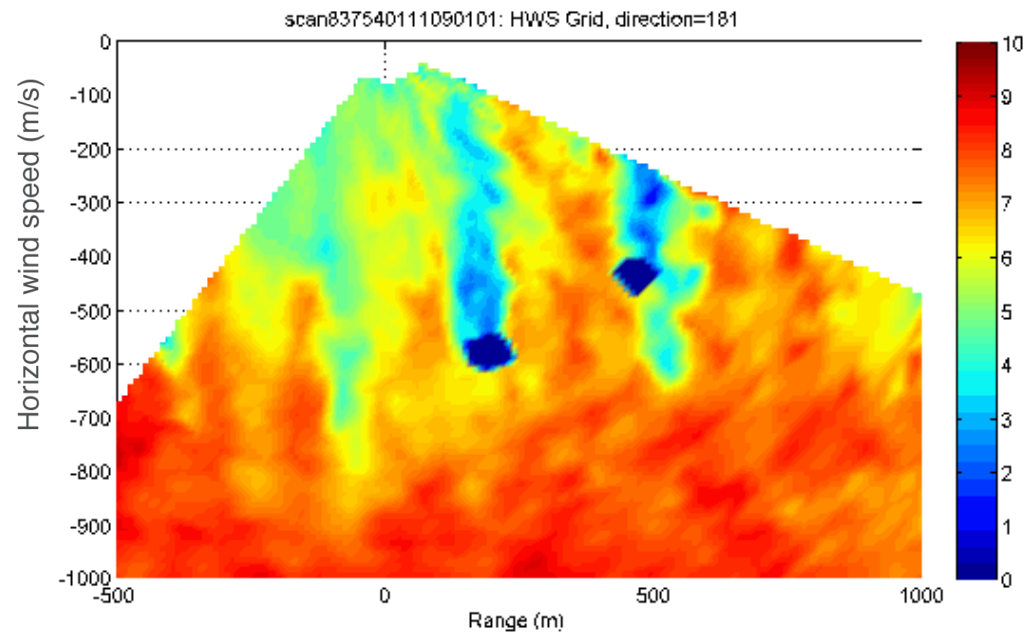
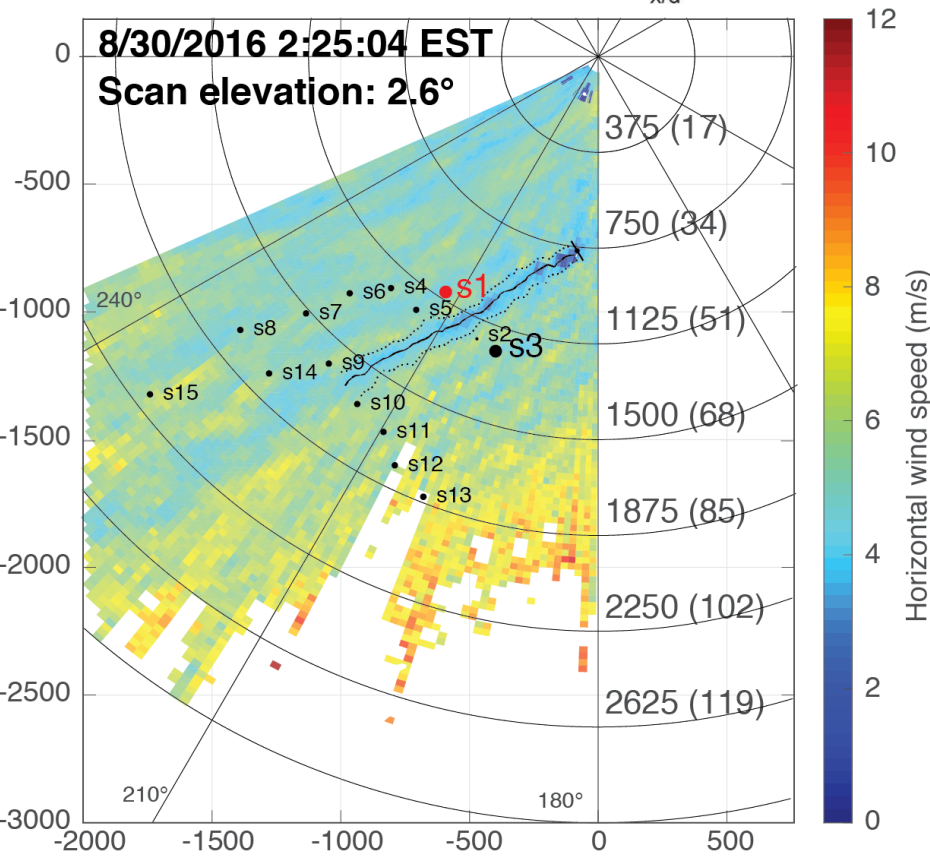
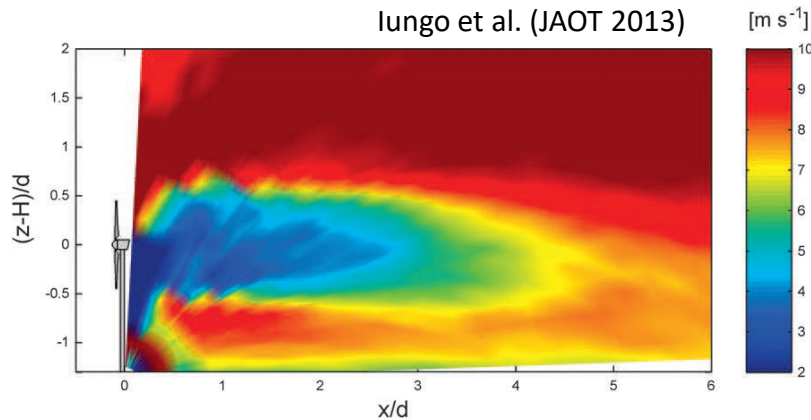


Horns Rev 2 (1/25/2016)

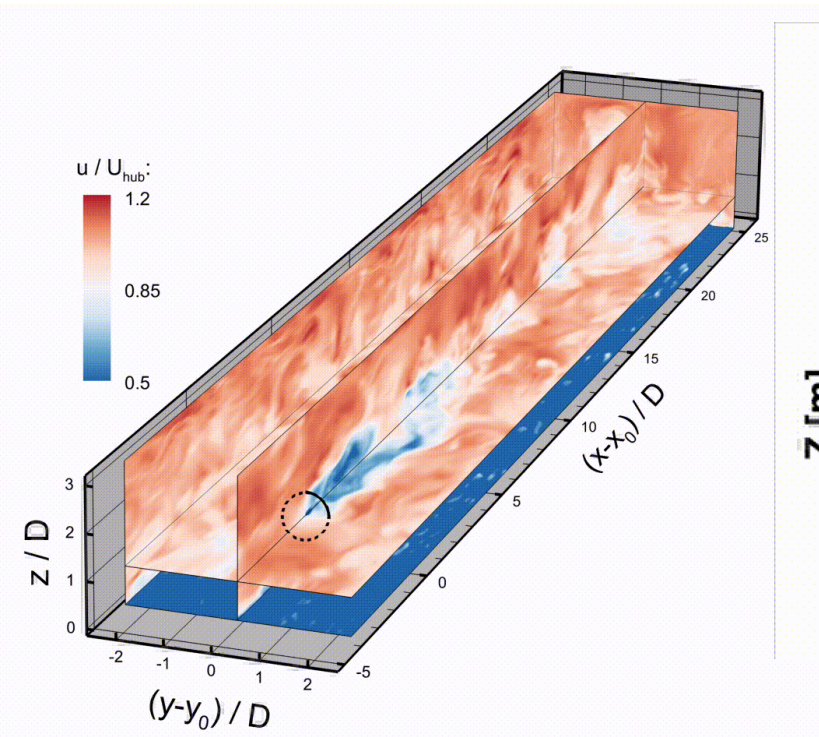




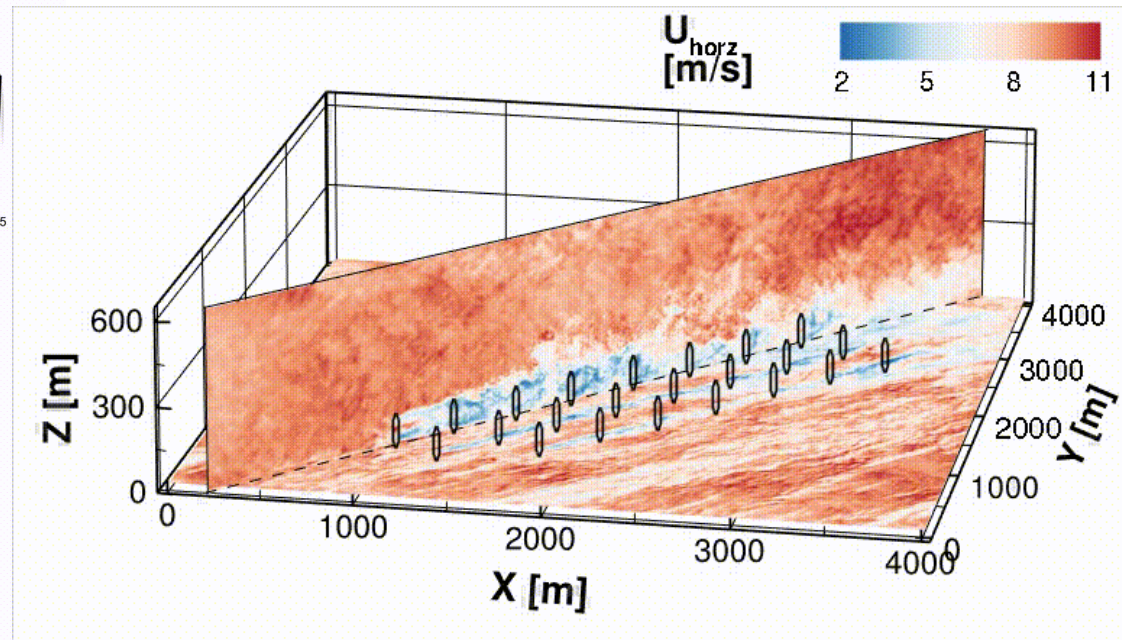
# Lidars show wind speed deficit in wakes



# Large-Eddy Simulation (LES) of single- and multi-turbine wakes



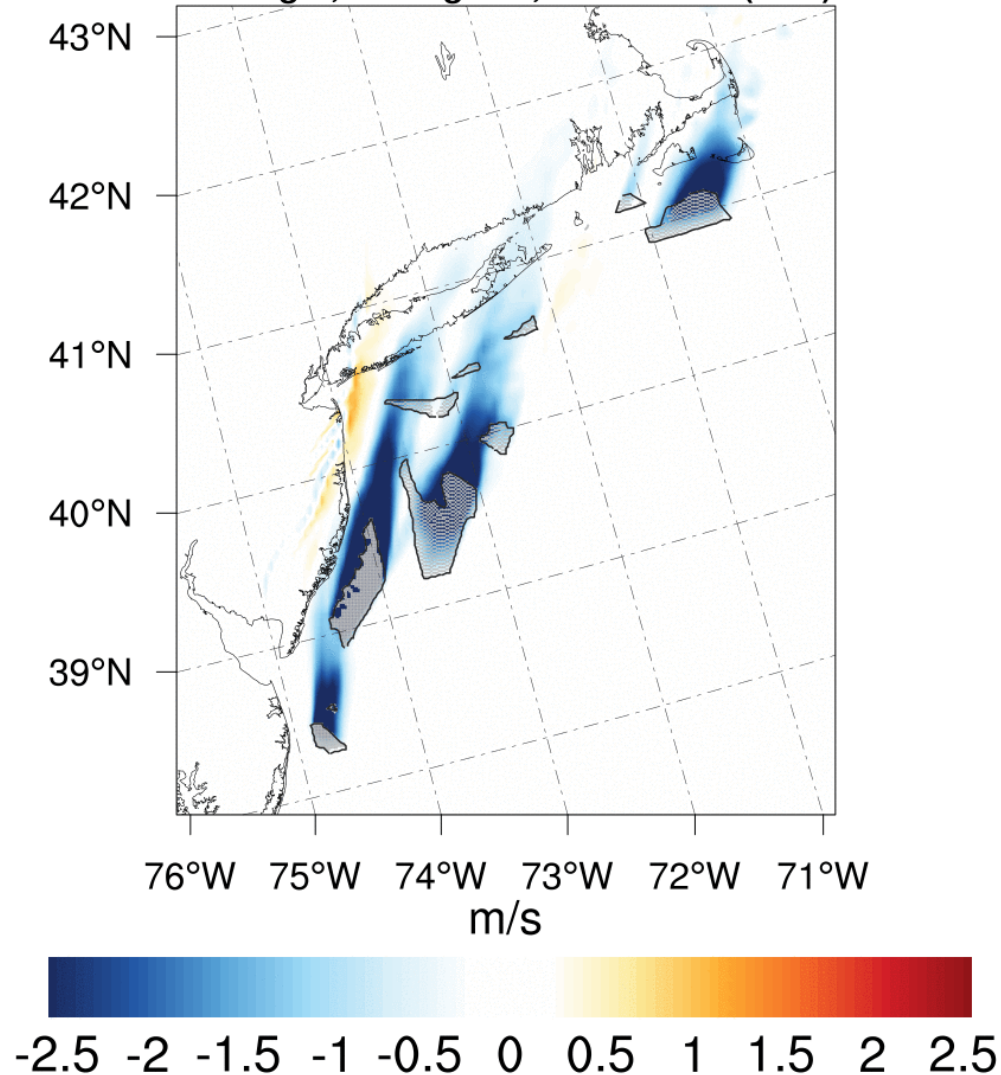
In-house code WiTTS  
(Wind Turbine and  
Turbulence Simulator)



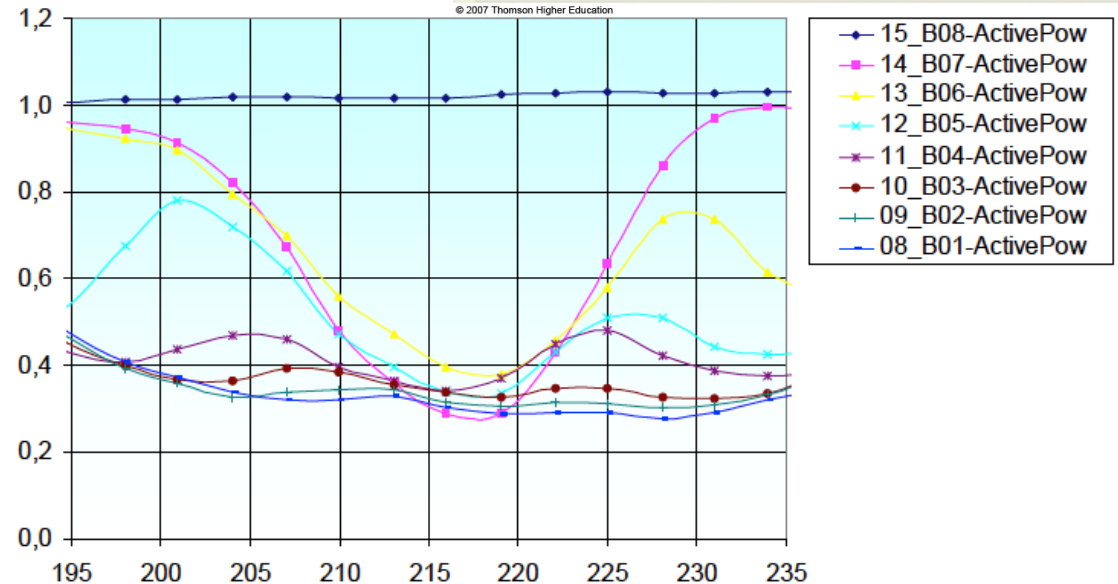
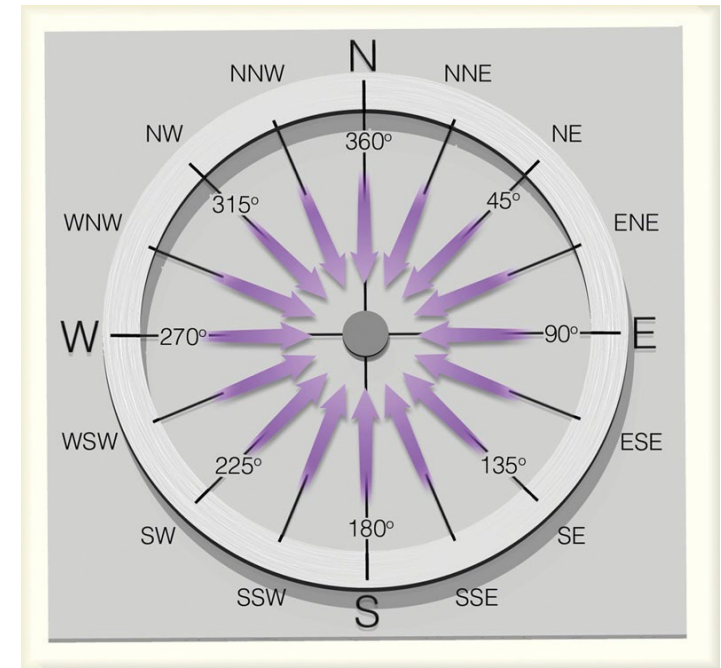
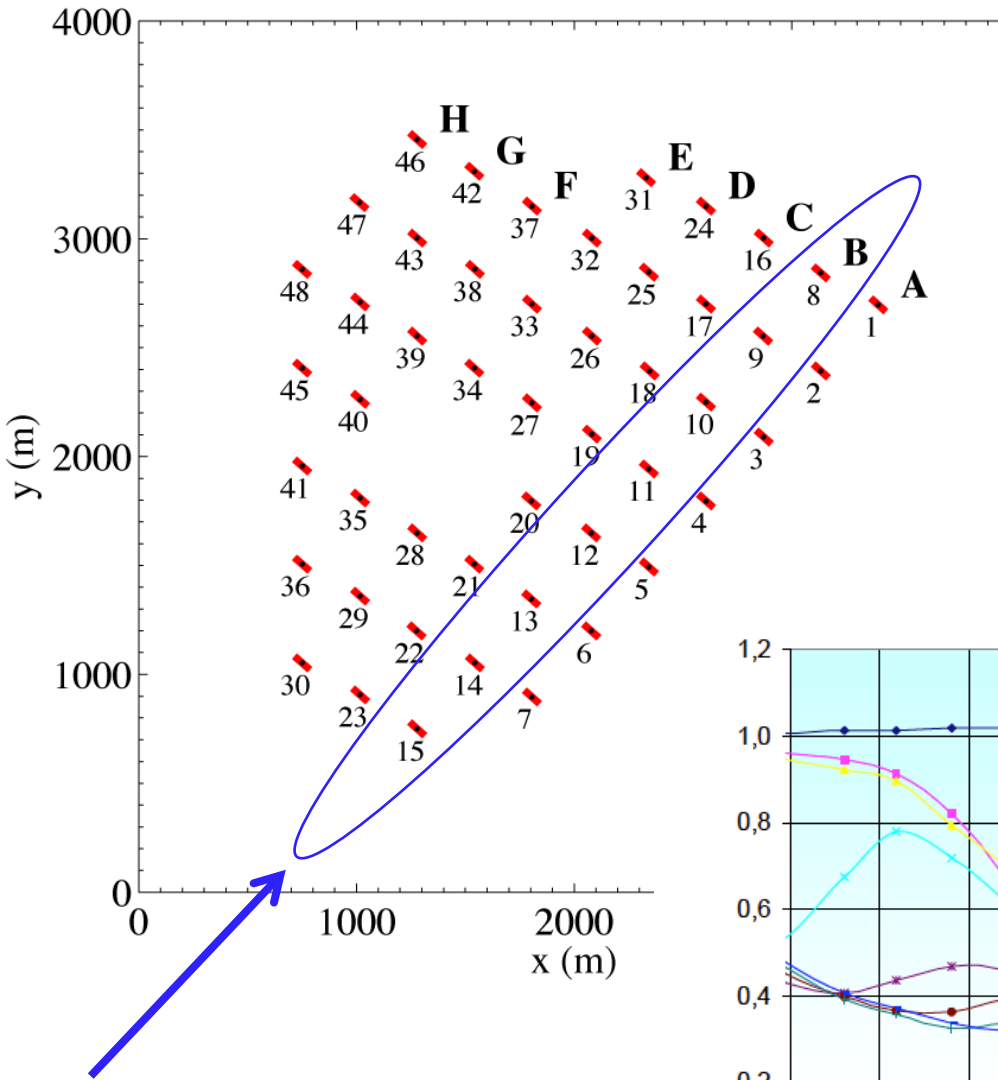
OpenFOAM-based SOWFA  
(Software for Offshore/onshore  
Wind Farm Applications)

# WRF-simulated wind speed deficit

Wind speed changes (turbine wakes) due to the wind farms  
at the hub height, on Aug 2nd, 2018 at hr 0 (UTC)

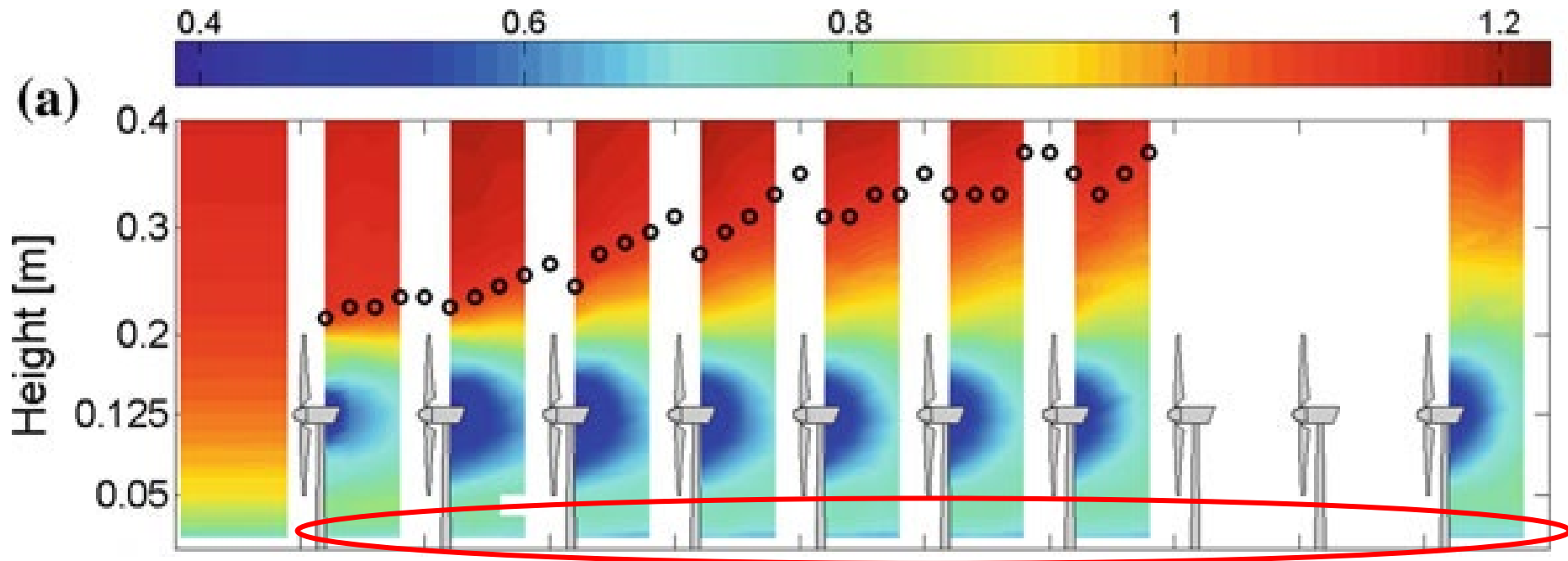


# Wind speed deficit = Reduced power



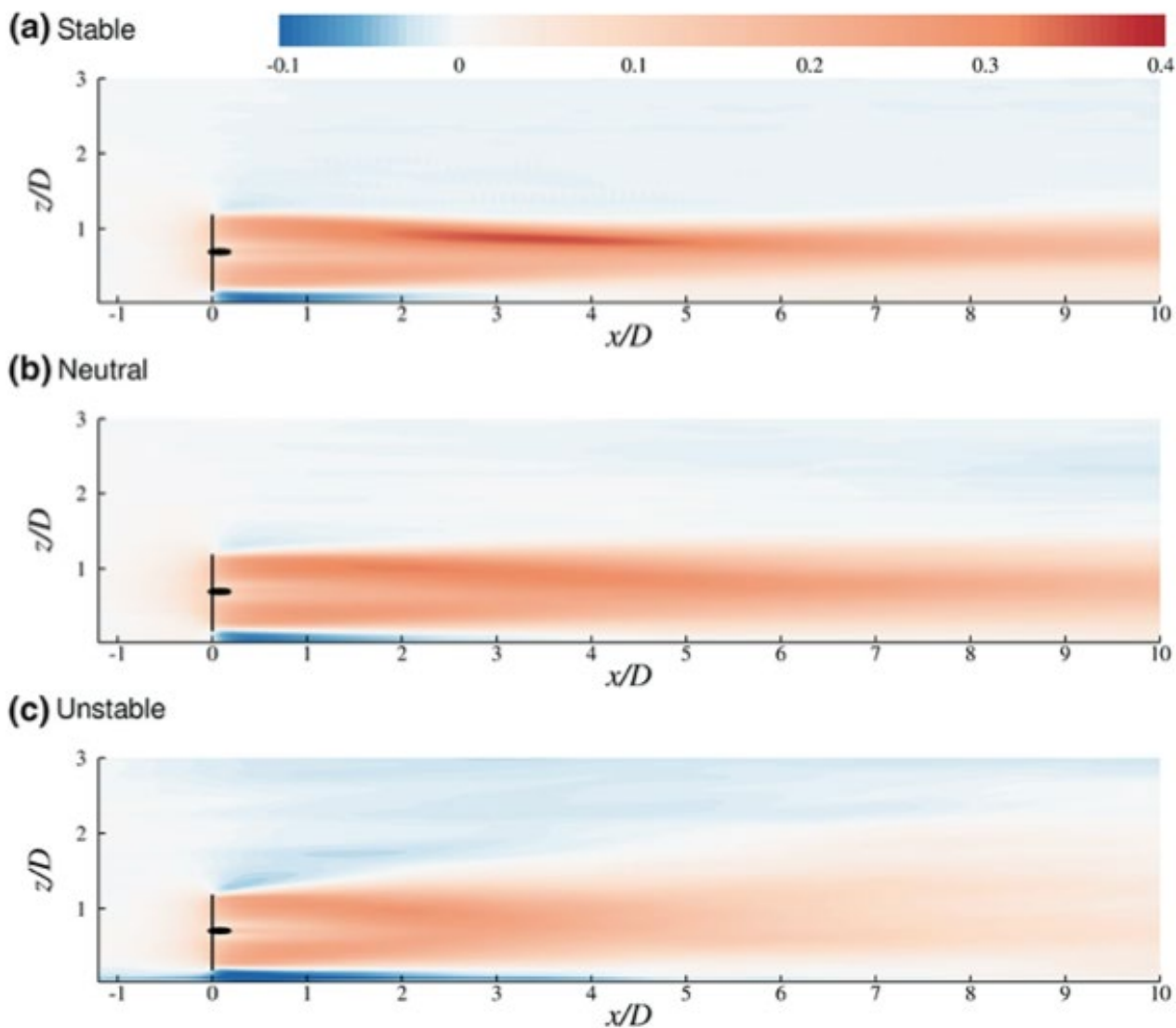


# Wind speed deficit: Wind tunnel



Wind speed deficit reaches ground

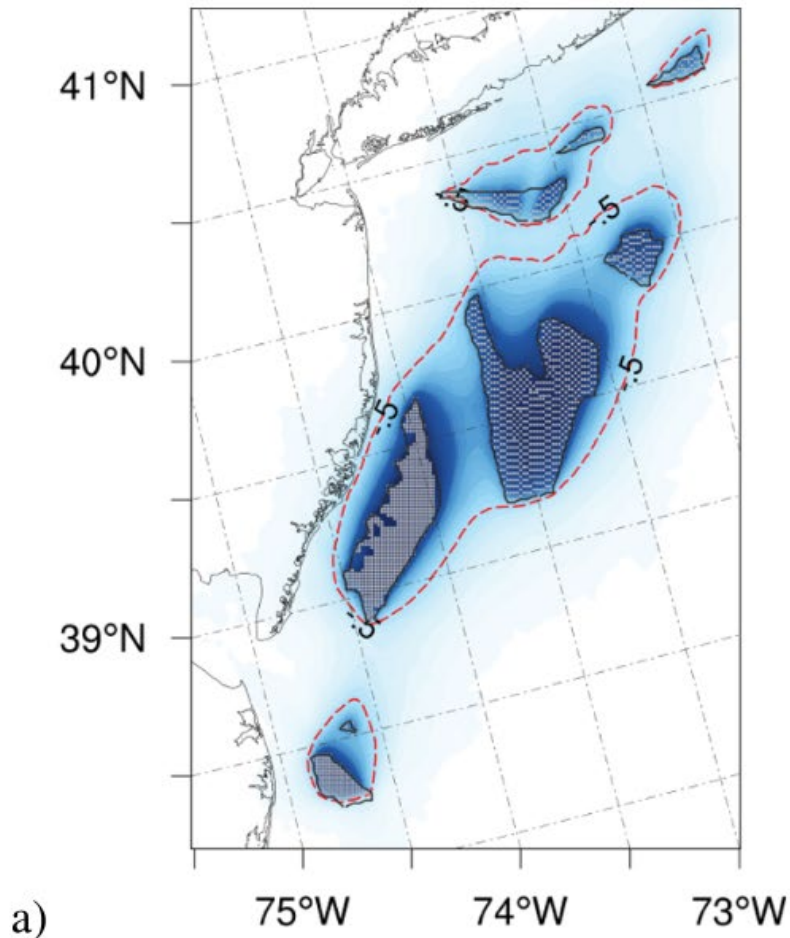
# Wind speed deficit: LES



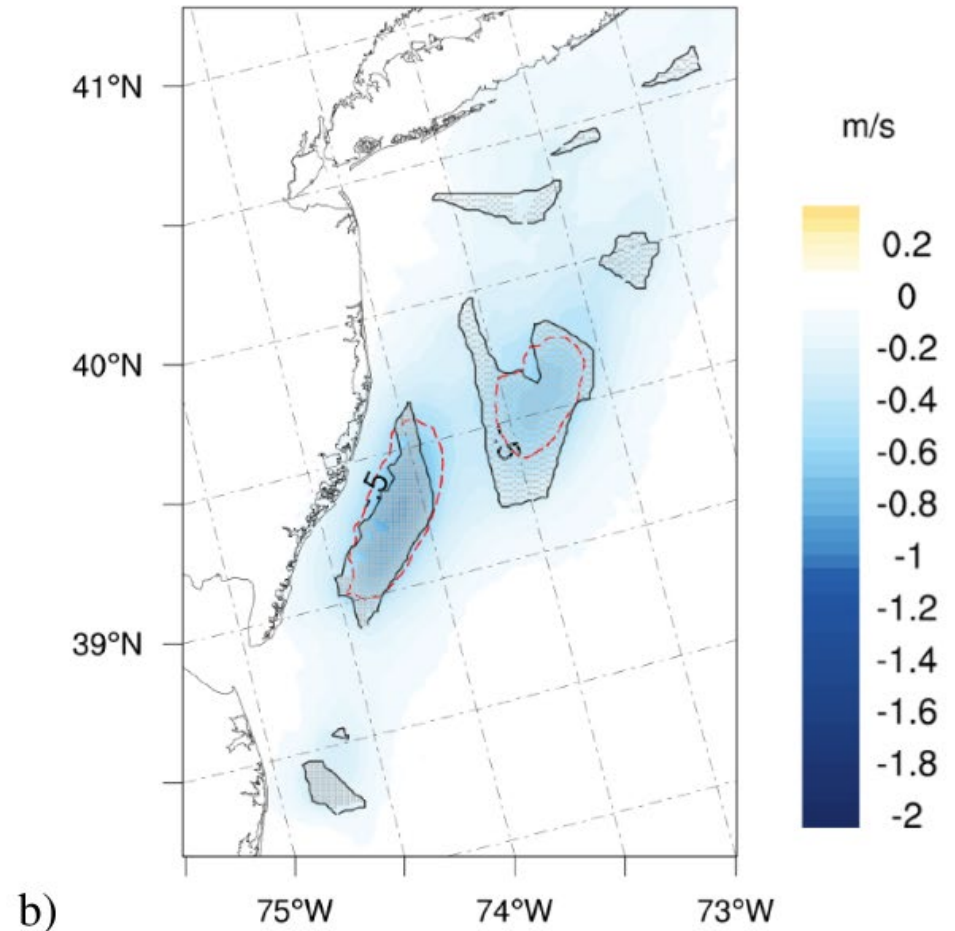


# Wind speed deficit: WRF

Hub height (120 m)

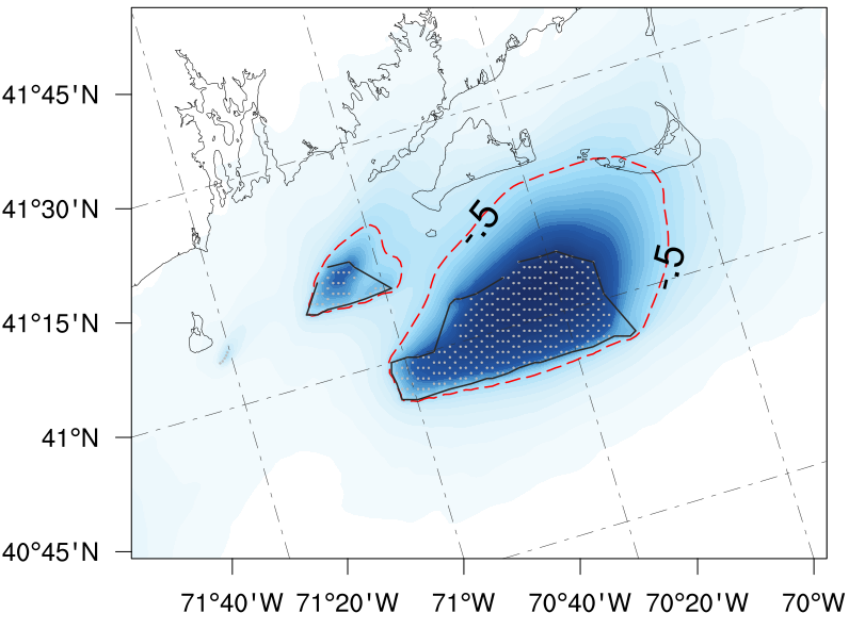


Surface (3.5 m)

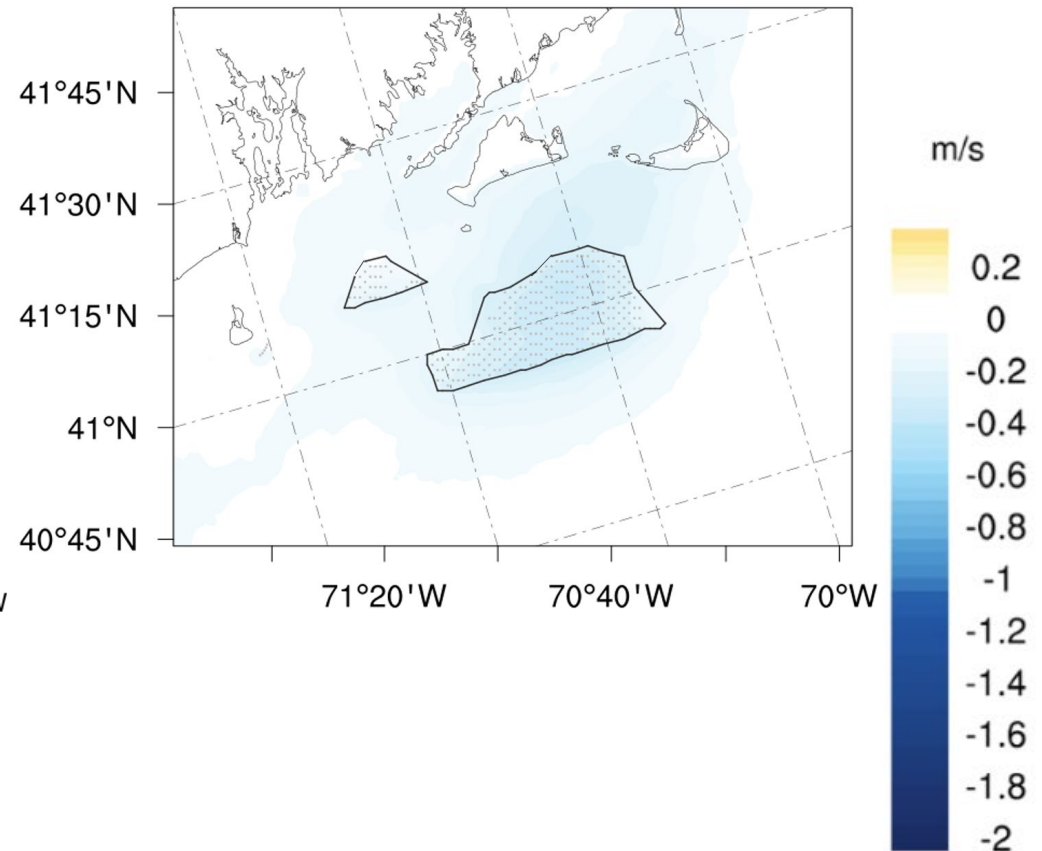


# Wind speed deficit: WRF

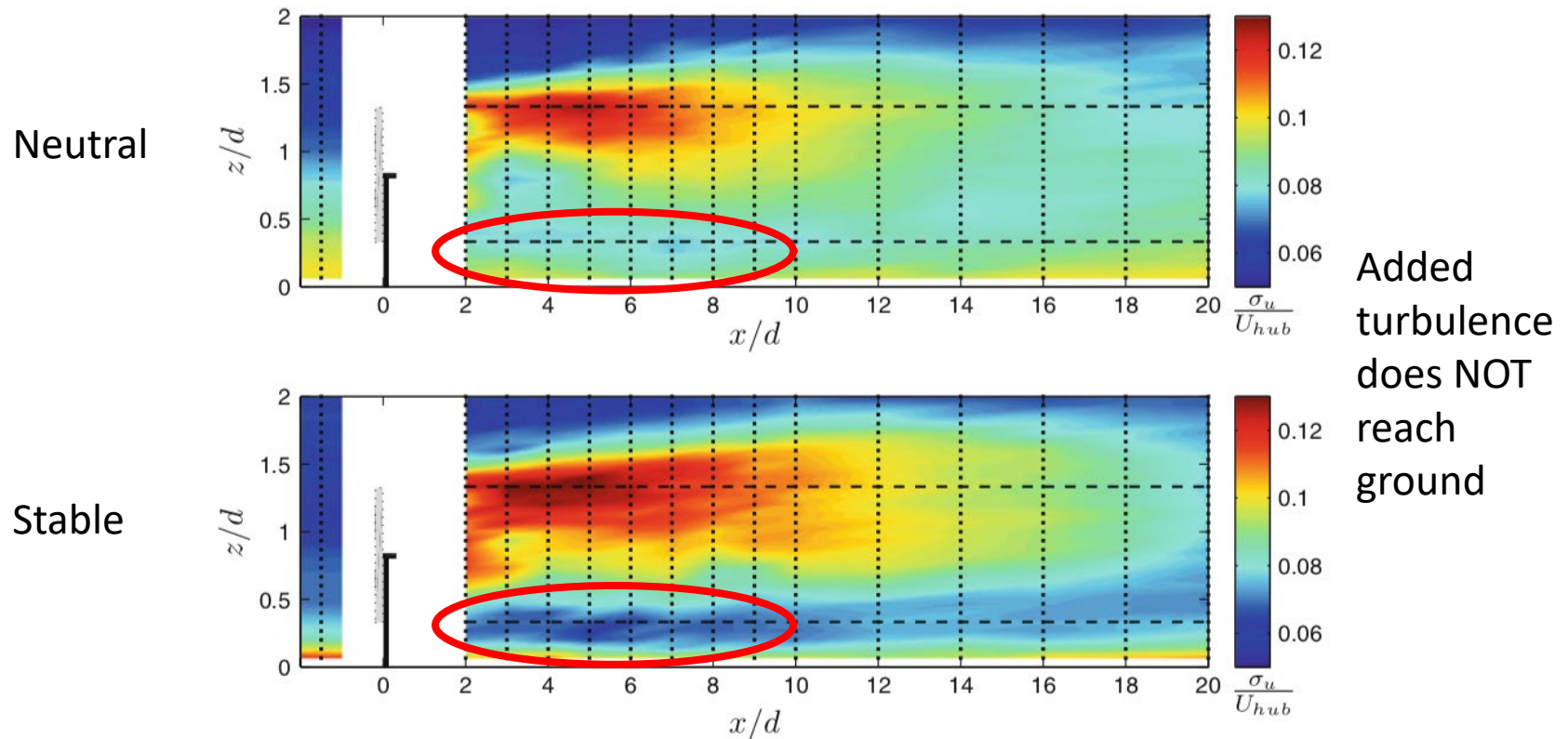
Hub height (120 m)



Surface (3.5 m)

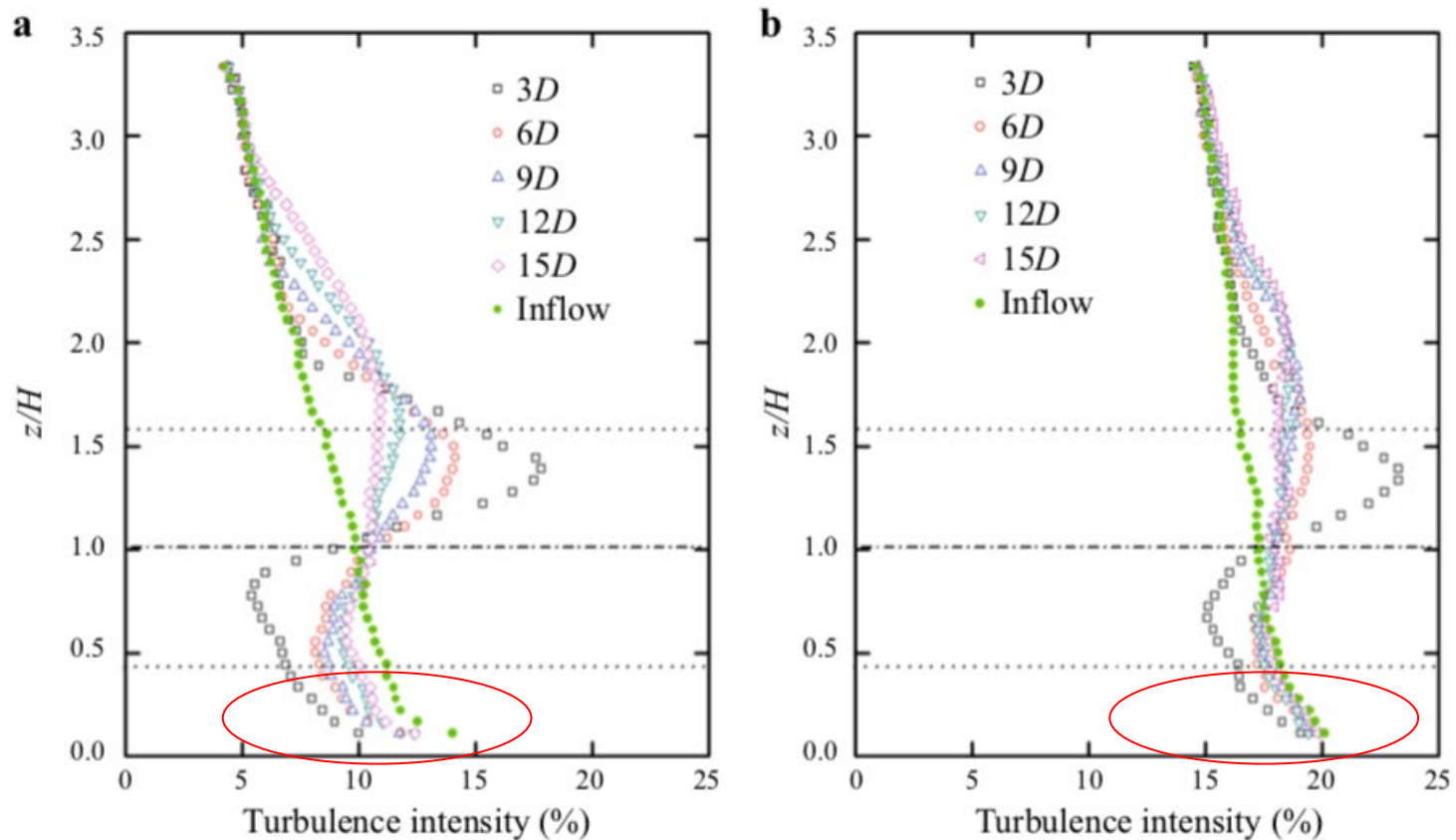


# Added turbulence: Wind tunnel experiments



**Fig. 7** Turbulence intensity distribution downwind of the turbine at zero span in the neutral (*top*) and in the stable stratified (*bottom*) boundary layer. Horizontal-dashed lines represent the turbine bottom and top tip heights and dots indicate measurement locations

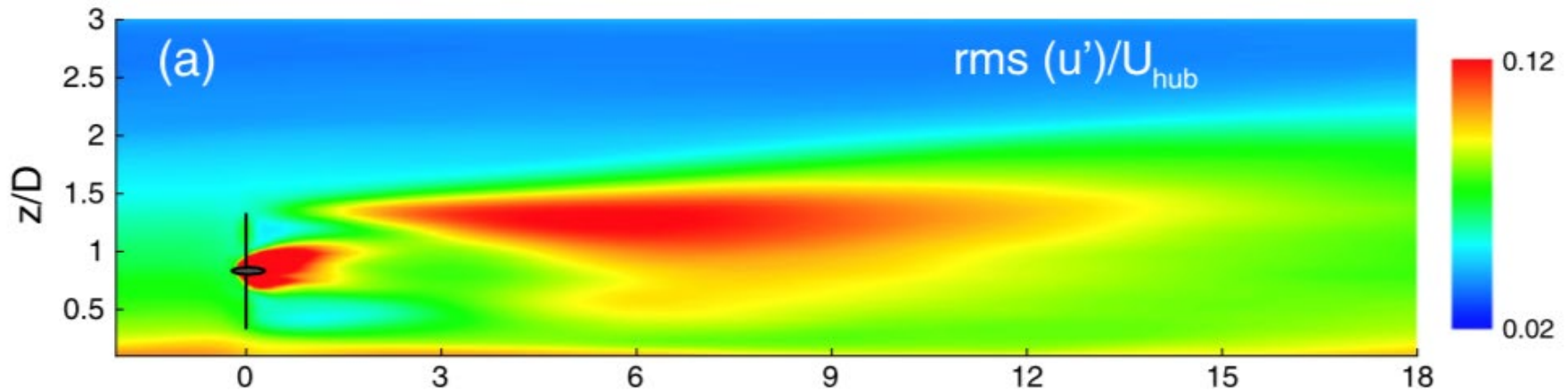
# Added turbulence: More wind tunnel experiments



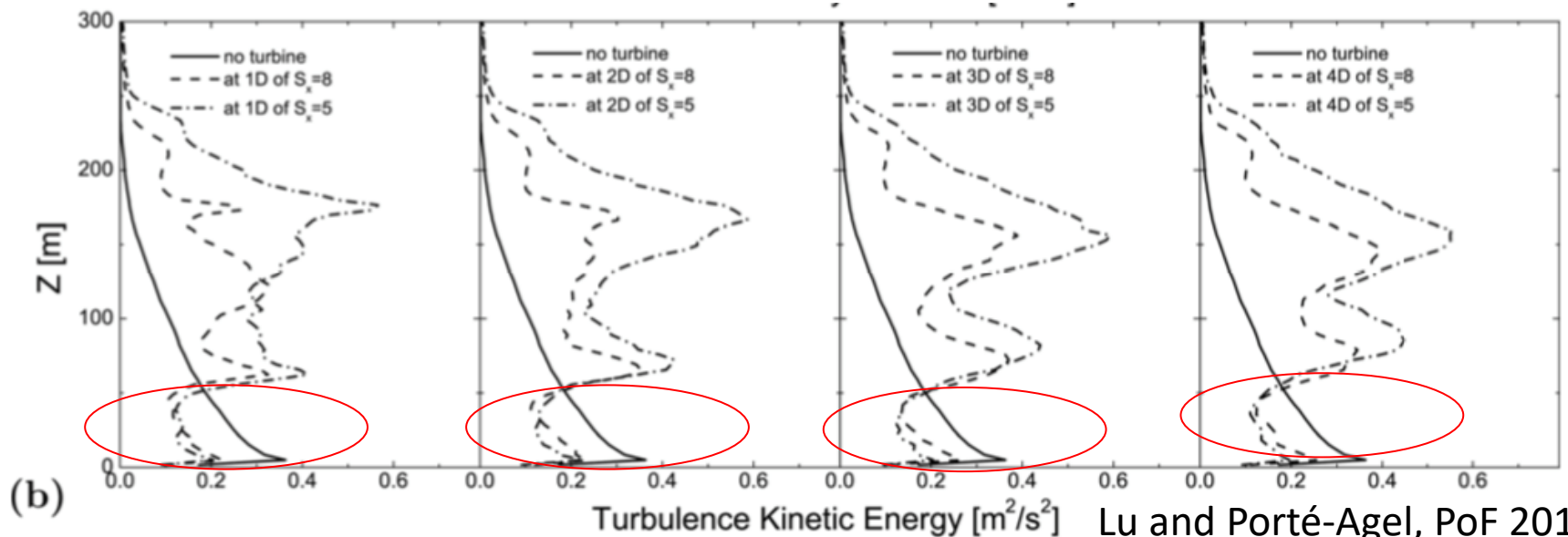
**Fig. 8** Measured turbulence intensity profiles at different downstream locations. **a** Low turbulence inflow case; **b** high turbulence inflow case



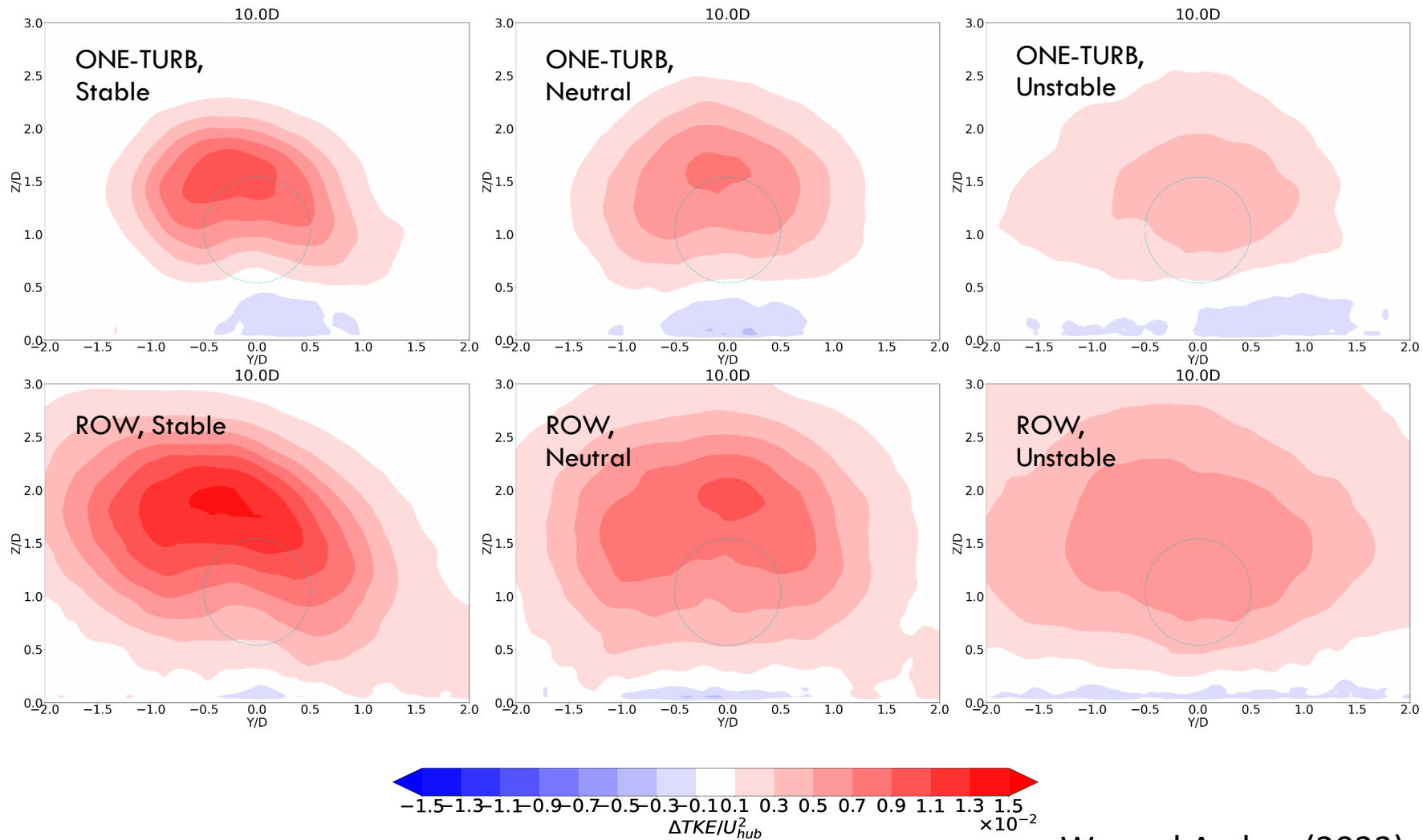
# Added turbulence: LES



Xie and Archer, WE 2015

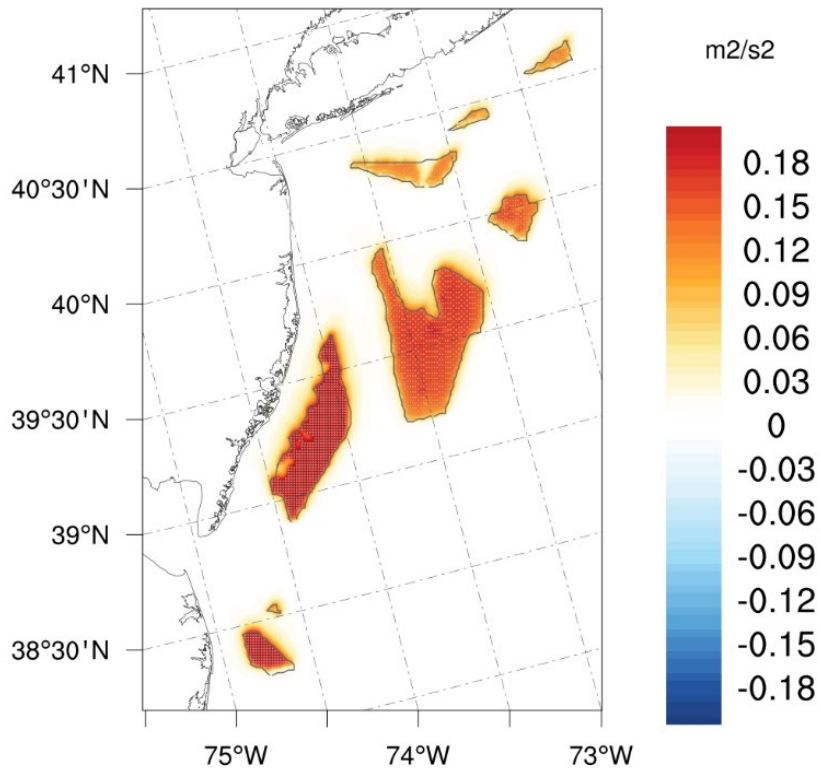


# Added TKE: LES

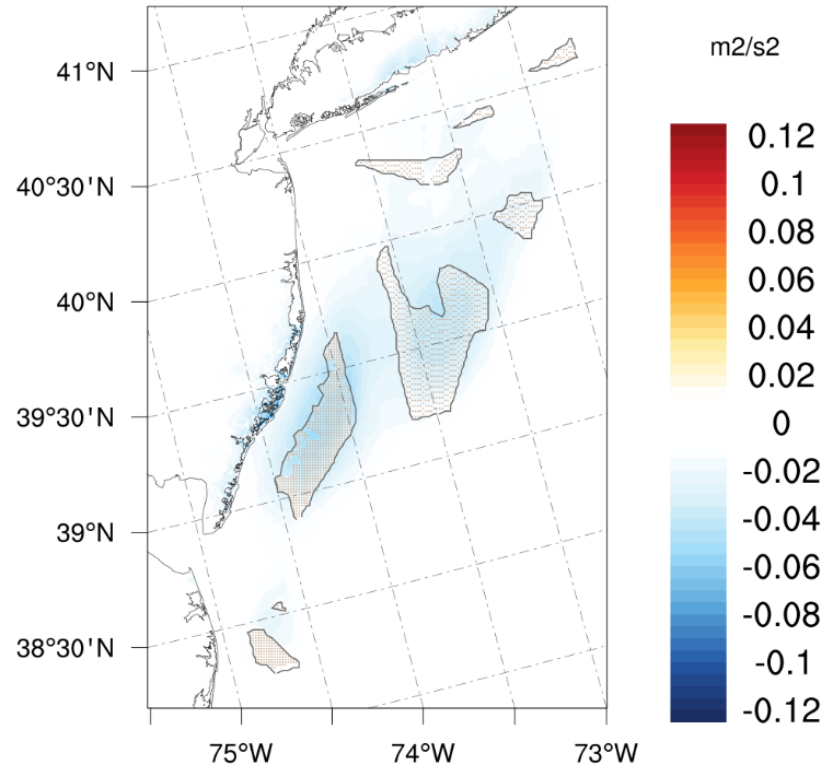


# Added TKE: WRF

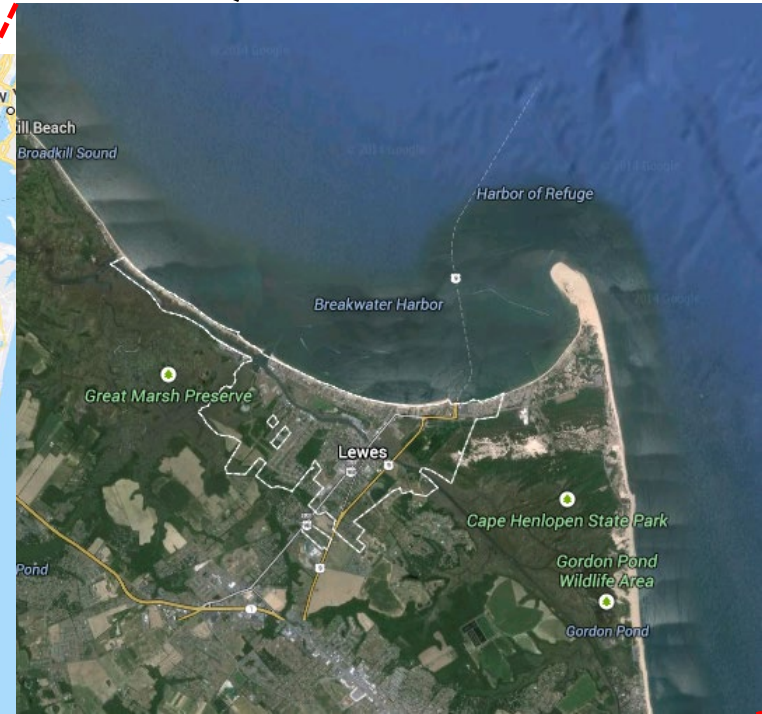
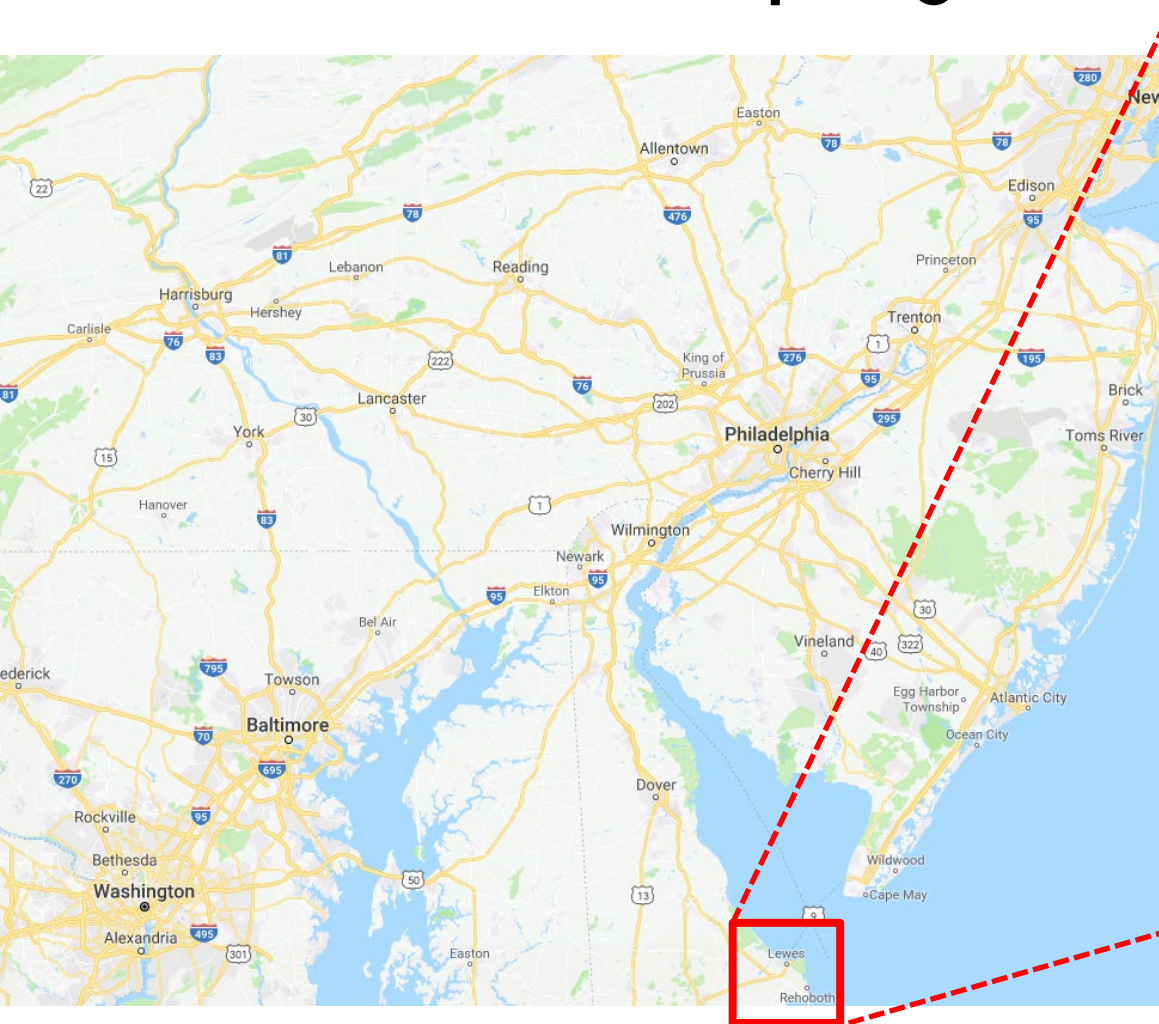
**Near top of the rotor**



**At the surface**



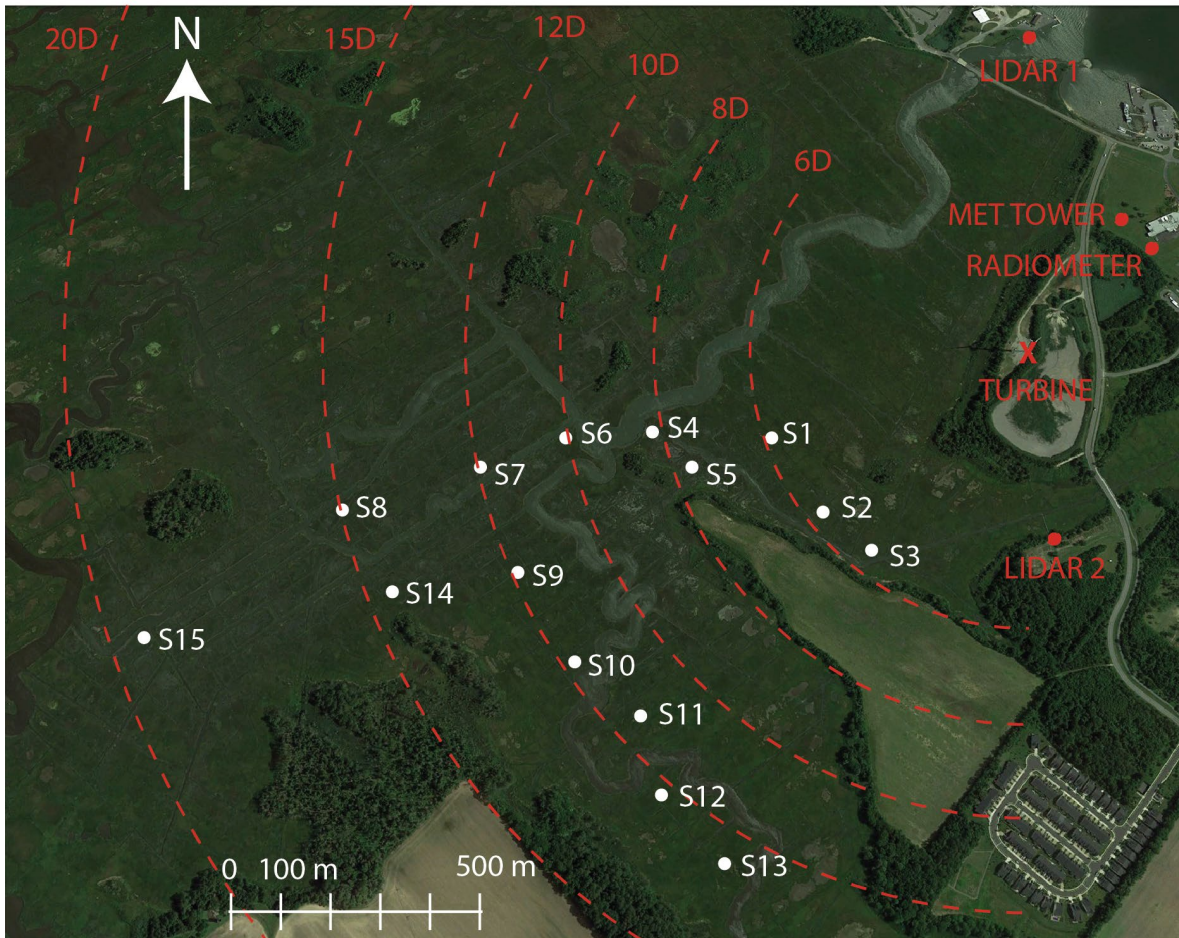
# The VERTical Enhanced miXing (VERTeX) field campaign in Lewes, DE



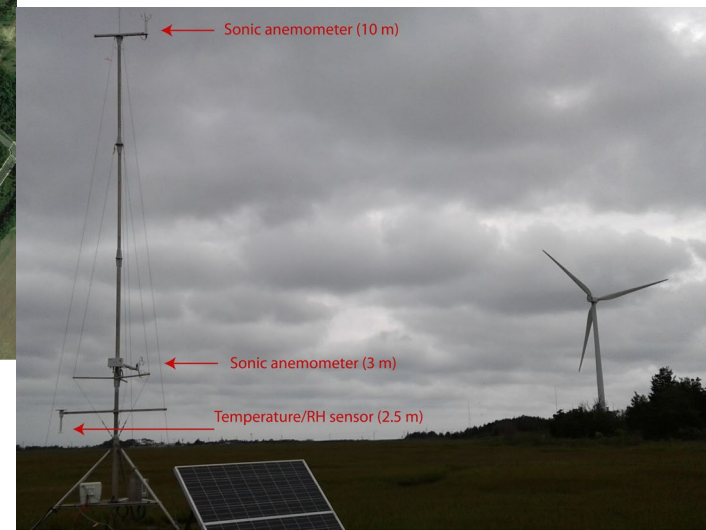
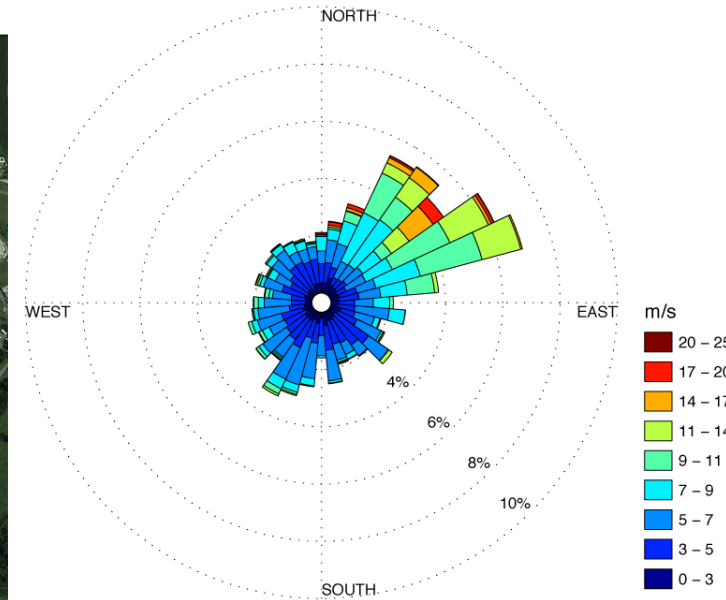
<http://www.ceoe.udel.edu/lewesturbine/index.shtml>



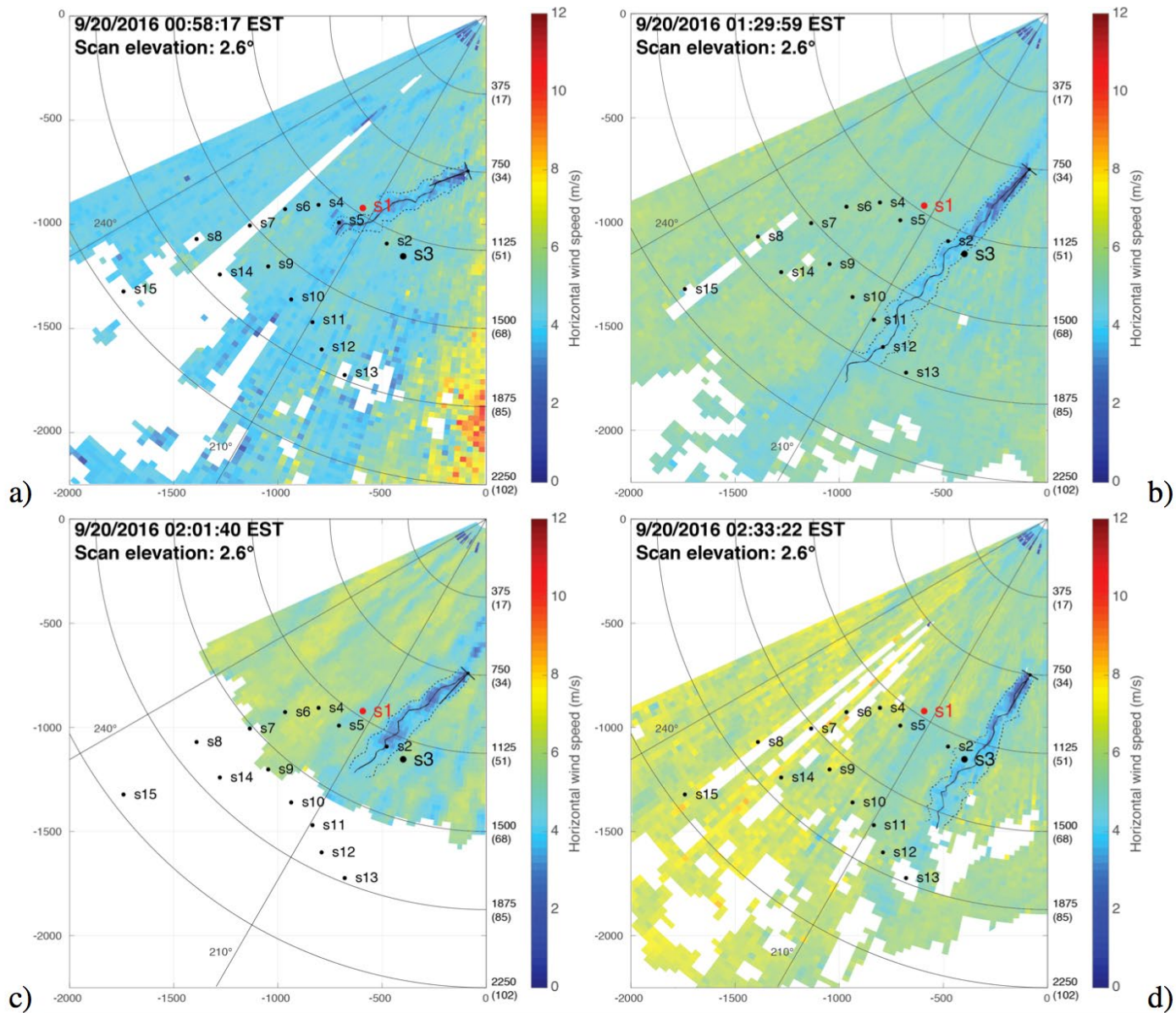
# Layout of the VERTEX campaign



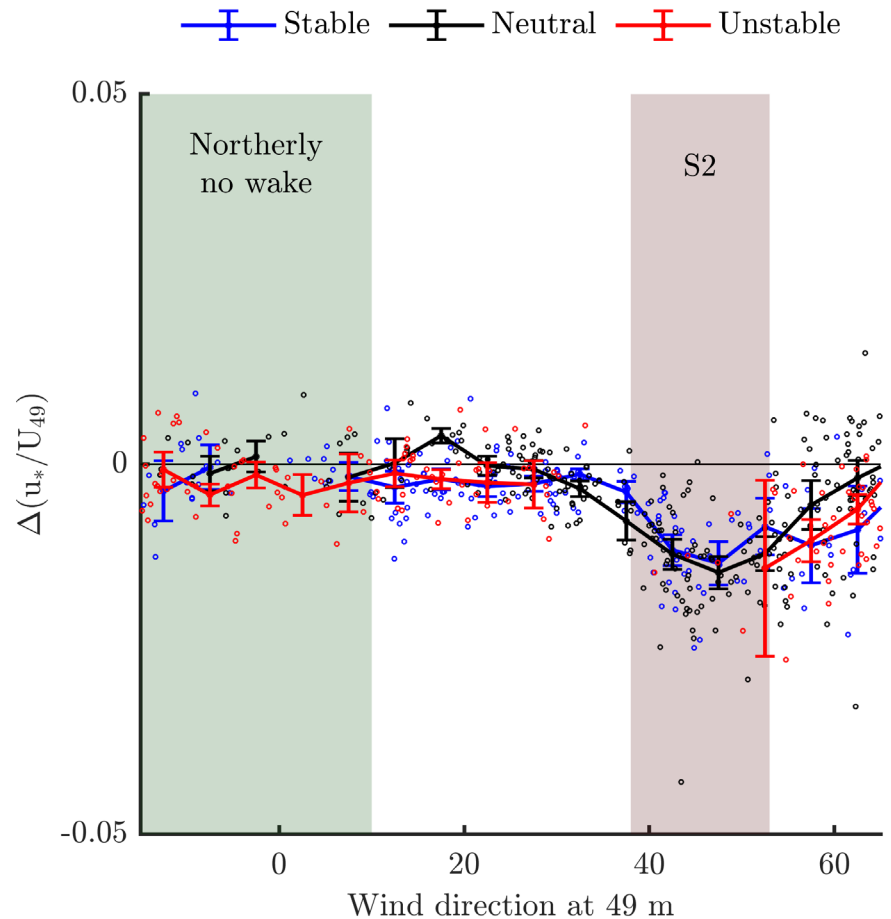
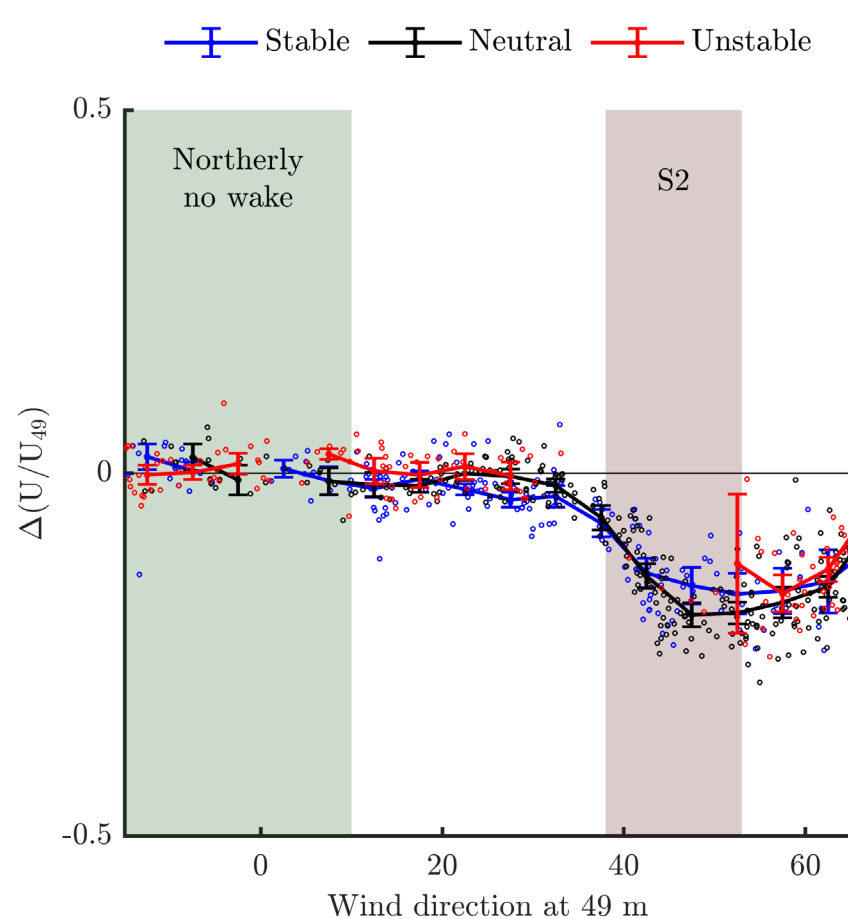
Lewes, SED tower, 49-m wind speed, 45-m wind direction, September



# Neutral case: 20 September 2016



# All cases: Wind speed and $u_*$ are reduced under the wake





# Summary of VERTEX findings

$\Delta(U/U_{49})$		S2-S1	S3-S1	S10-S7
No-wake conditions	Stable	0.006 (0.032)	-0.012 (0.042)	0.032 (0.039)
	Neutral	-0.001 (0.028)	-0.030 (0.043)	0.027 (0.029)
	Unstable	0.003 (0.026)	-0.031 (0.029)	0.031 (0.029)
Wake conditions	Stable	-0.123 (0.053)	-0.126 (0.051)	-0.125 (0.055)
	Neutral	-0.132 (0.056)	-0.128 (0.048)	-0.116 (0.052)
	Unstable	-0.156 (0.051)	-0.090 (0.037)	-0.137 (0.053)

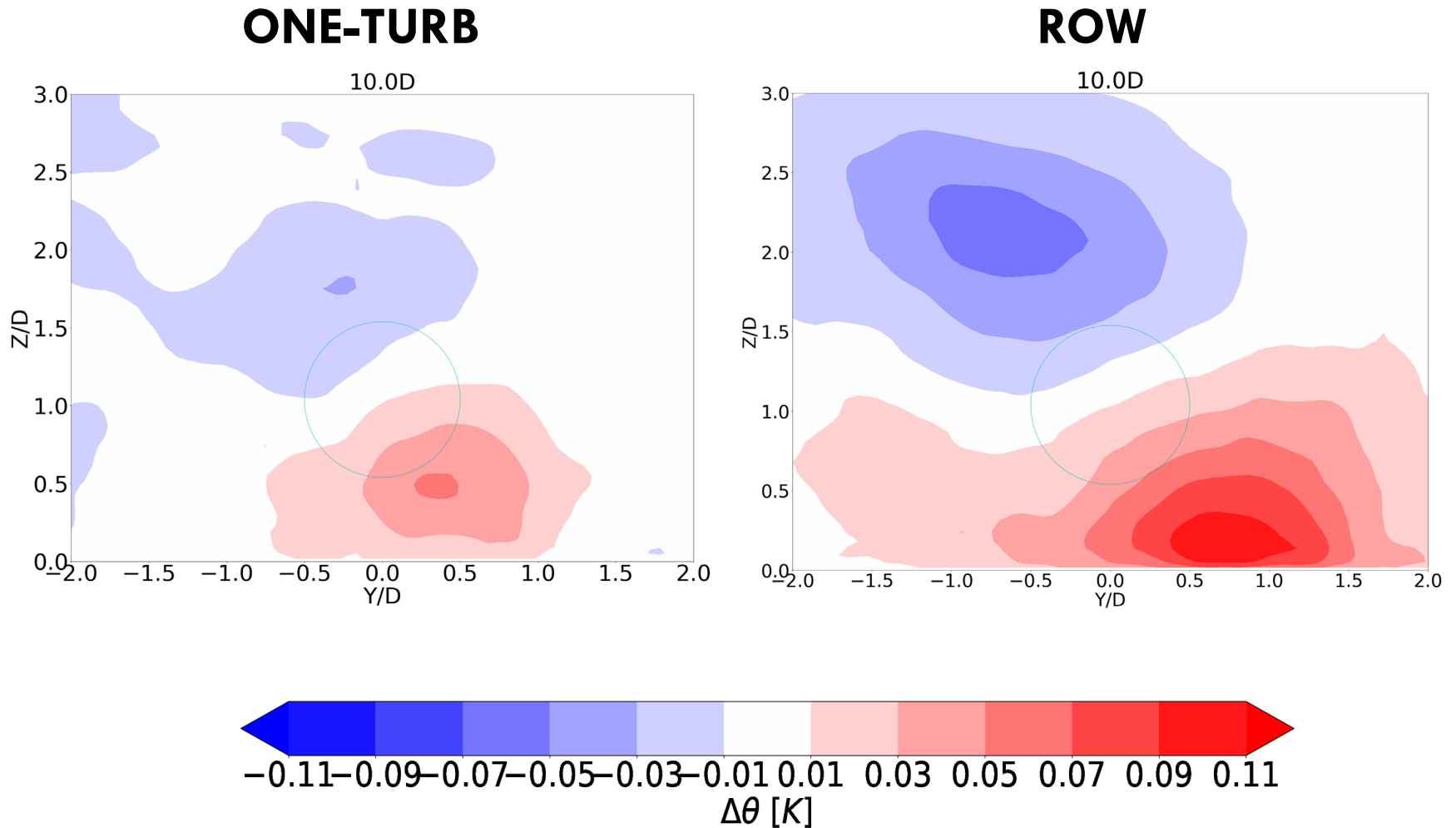


# Summary of VERTEX findings

$\Delta(U/U_{49})$		S2-S1	S3-S1	S10-S7	$\Delta(u^*/U_{49})$		S2-S1	S3-S1	S10-S7
No-wake conditions	Stable	0.006 (0.032)	-0.012 (0.042)	0.032 (0.039)	No-wake conditions	Stable	-0.002 (0.004)	-0.001 (0.005)	-0.002 (0.003)
	Neutral	-0.001 (0.028)	-0.030 (0.043)	0.027 (0.029)		Neutral	-0.002 (0.003)	-0.001 (0.003)	-0.002 (0.004)
	Unstable	0.003 (0.026)	-0.031 (0.029)	0.031 (0.029)		Unstable	-0.001 (0.004)	-0.001 (0.004)	-0.001 (0.004)
Wake conditions	Stable	-0.123 (0.053)	-0.126 (0.051)	-0.125 (0.055)	Wake conditions	Stable	-0.010 (0.006)	-0.008 (0.006)	-0.004 (0.007)
	Neutral	-0.132 (0.056)	-0.128 (0.048)	-0.116 (0.052)		Neutral	-0.010 (0.006)	-0.008 (0.005)	-0.002 (0.006)
	Unstable	-0.156 (0.051)	-0.090 (0.037)	-0.137 (0.053)		Unstable	-0.012 (0.007)	-0.007 (0.004)	-0.005 (0.005)

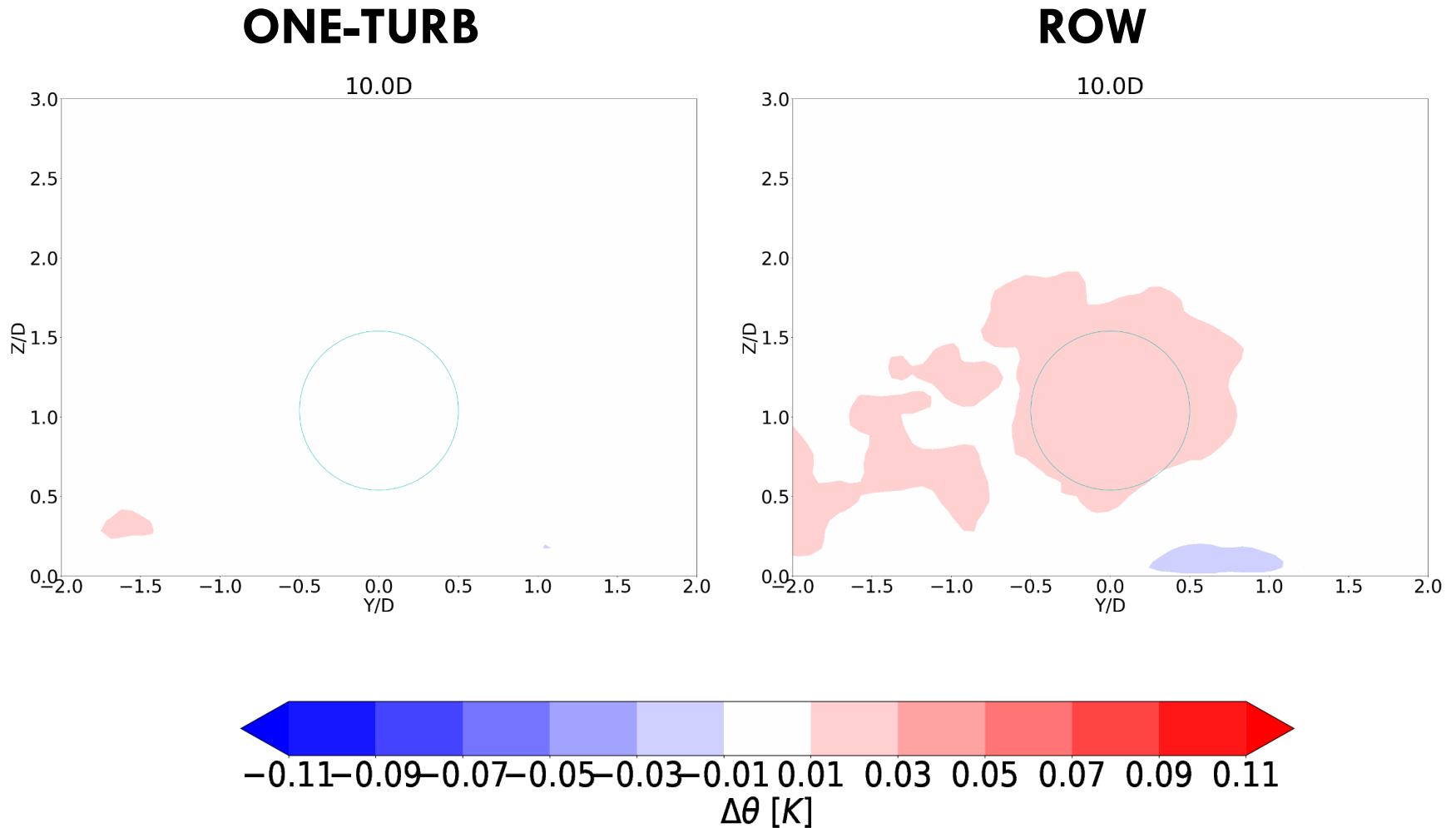
$\Delta(\overline{w'T'_v})$		S2-S1	S3-S1	S10-S7	$\Delta(T)$		S2-S1	S3-S1	S10-S7
No-wake conditions	Stable	0.000 (0.013)	-0.005 (0.013)	0.002 (0.007)	No-wake conditions	Stable	-0.12 (0.12)	-0.11 (0.12)	0.08 (0.15)
	Neutral	0.003 (0.010)	-0.002 (0.009)	0.003 (0.014)		Neutral	-0.11 (0.09)	-0.07 (0.07)	0.10 (0.08)
	Unstable	-0.004 (0.016)	-0.009 (0.013)	-0.003 (0.006)		Unstable	-0.01 (0.10)	-0.06 (0.07)	0.11 (0.11)
Wake conditions	Stable	-0.006 (0.006)	-0.003 (0.005)	-0.010 (0.055)	Wake conditions	Stable	0.09 (0.09)	0.10 (0.10)	0.19 (0.15)
	Neutral	-0.002 (0.004)	-0.002 (0.004)	-0.005 (0.005)		Neutral	-0.01 (0.06)	0.02 (0.06)	0.15 (0.06)
	Unstable	-0.003 (0.005)	-0.007 (0.008)	-0.006 (0.013)		Unstable	0.00 (0.07)	-0.07 (0.08)	0.09 (0.10)

# Temperature: LES (Stable)



Wu et al. (2023)

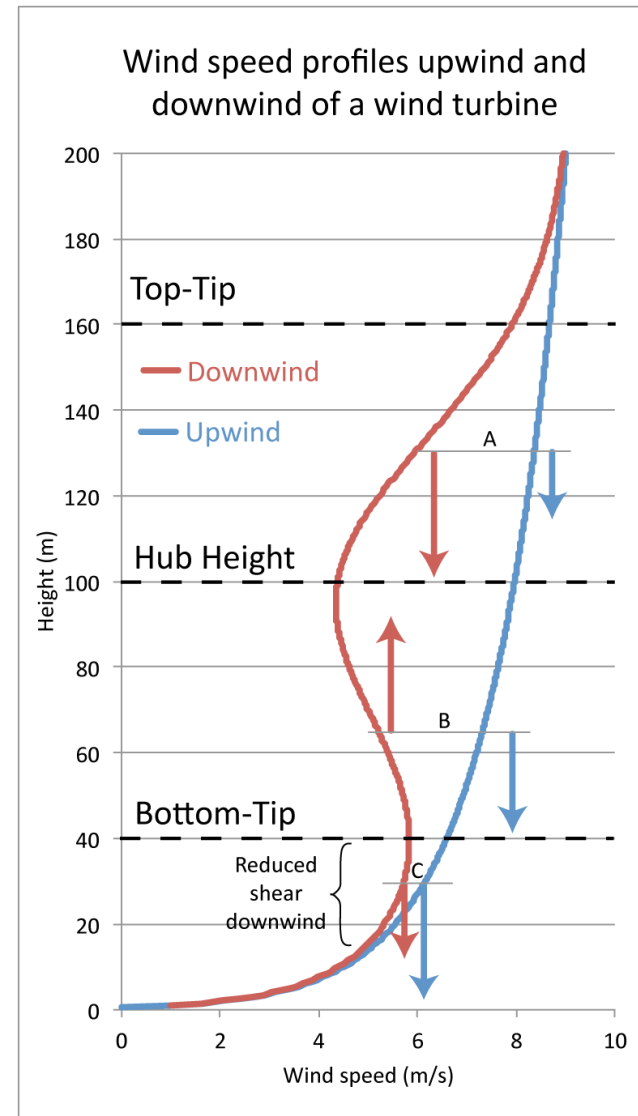
# Temperature: WRF-LES (Unstable)



# Wind turbines reduce vertical mixing and TKE near ground by reducing shear

- Wind shear below the rotor is reduced;
- Vertical momentum flux (arrows) is reduced (point C);
- Production of TKE is reduced;
- Vertical mixing is reduced or unchanged.

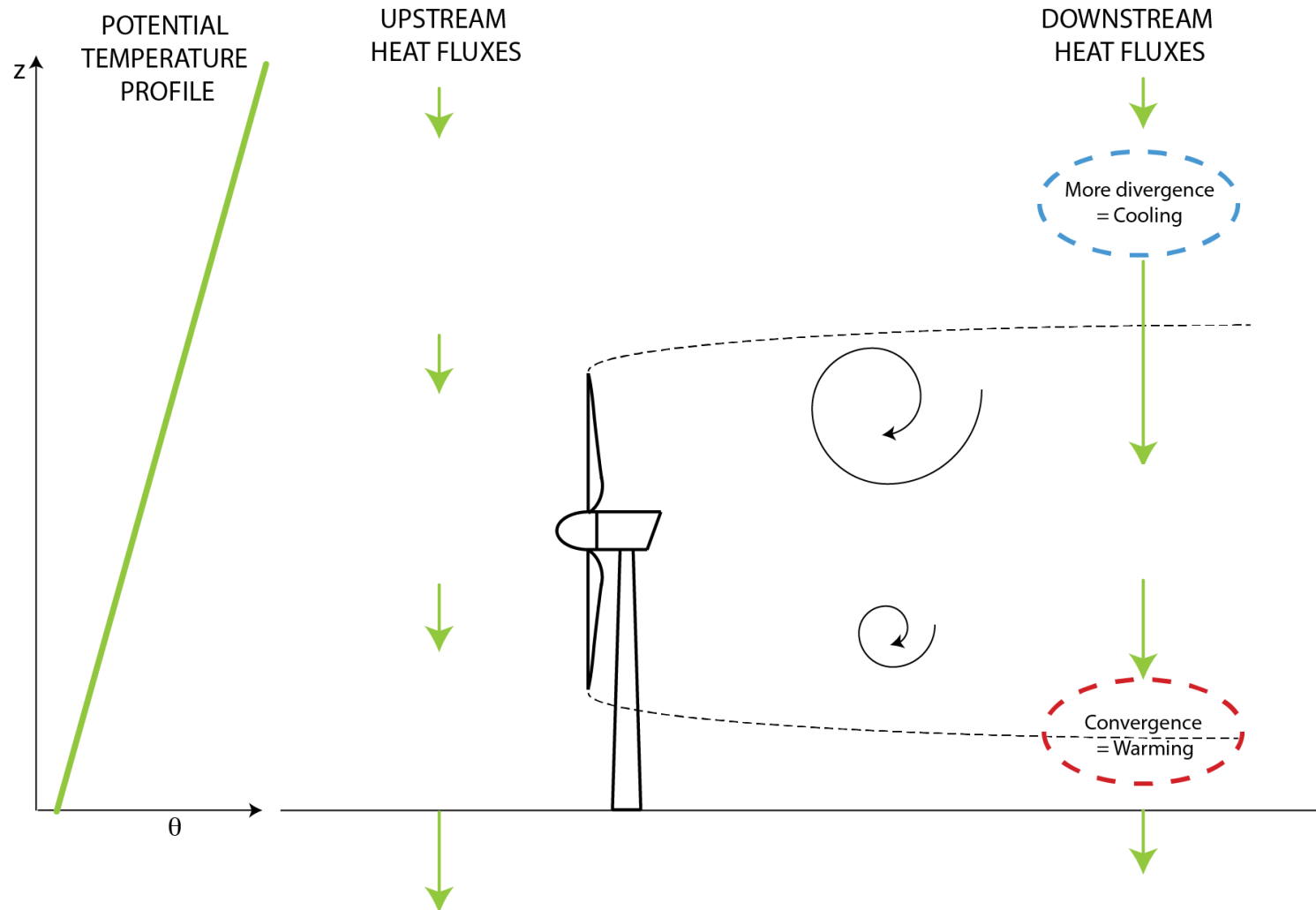
What causes the warming?





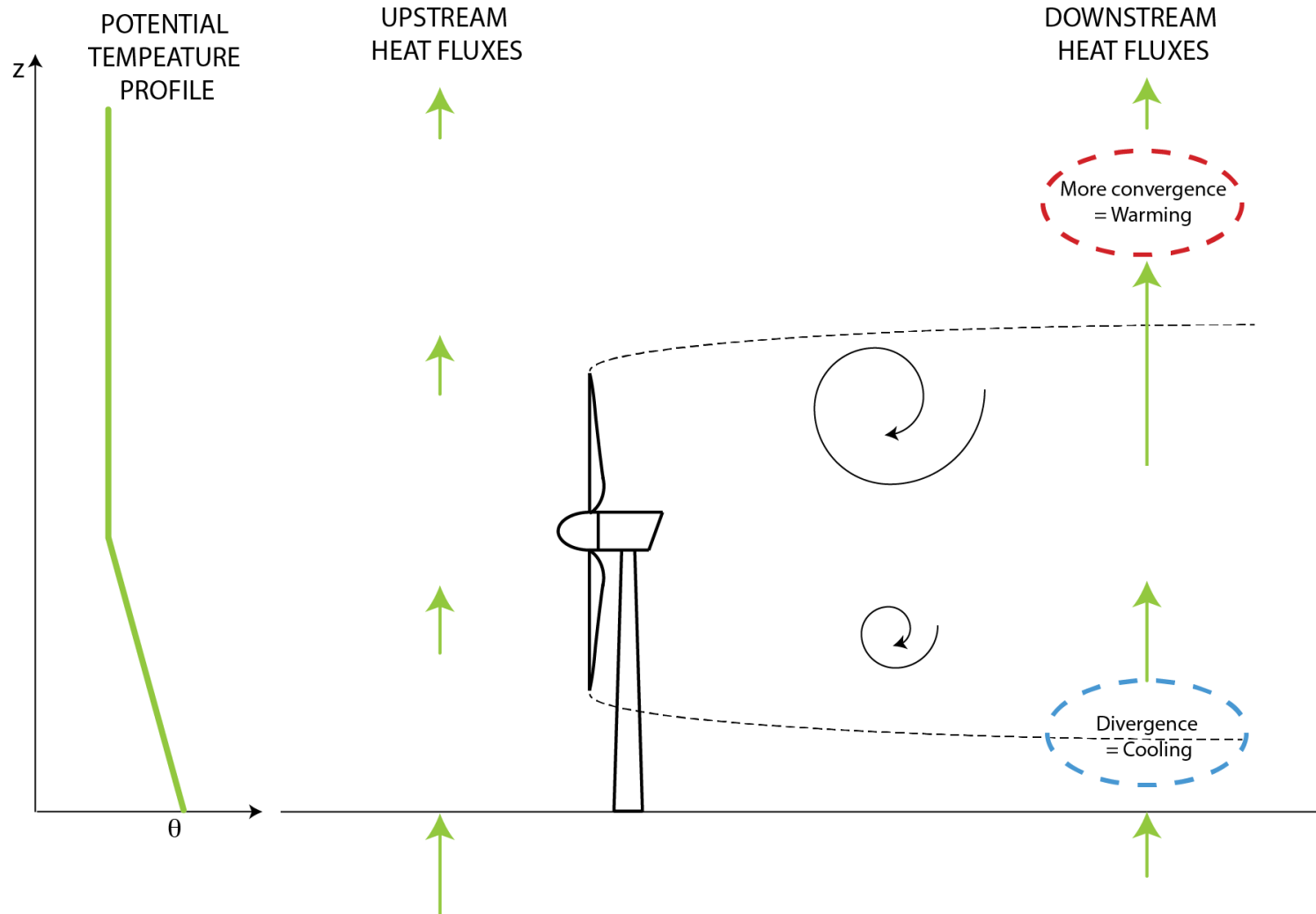
# Heat flux divergence – Stable case

STABLE CONDITIONS

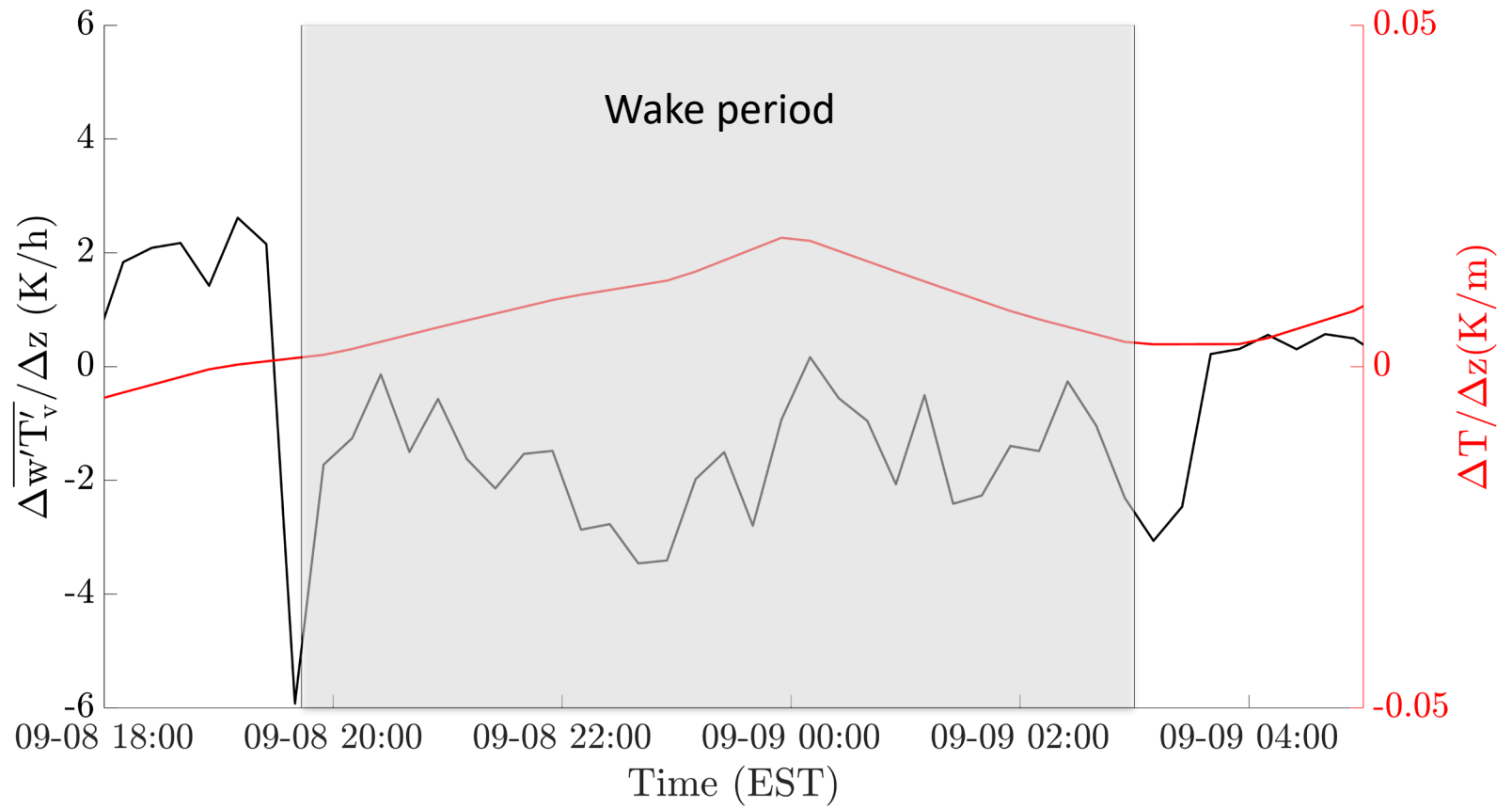


# Heat flux divergence – Unstable case

UNSTABLE CONDITIONS



# Heat flux divergence – VERTEX



# Energy budget equation

$$\partial_t \bar{\theta} = -\overline{U_j} \partial_j \bar{\theta} - \partial_j \overline{u_j' \theta'}$$

Advection

Convergence

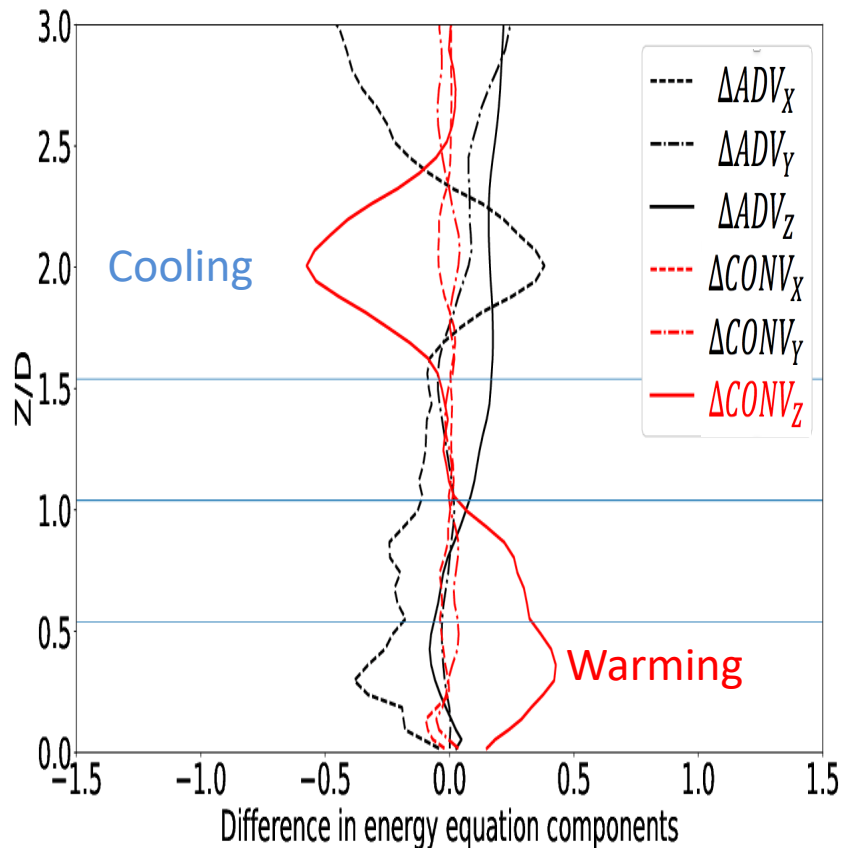
$$\begin{aligned} ADV_x &= -\frac{\bar{U} \frac{\partial \bar{\theta}}{\partial x}}{q_3/D} \\ ADV_y &= -\frac{\bar{V} \frac{\partial \bar{\theta}}{\partial y}}{q_3/D} \\ ADV_z &= -\frac{\bar{W} \frac{\partial \bar{\theta}}{\partial z}}{q_3/D} \end{aligned}$$

$$\begin{aligned} CONV_x &= -\frac{\frac{\partial \overline{u' \theta'}}{\partial x}}{q_3/D} \\ CONV_y &= -\frac{\frac{\partial \overline{v' \theta'}}{\partial y}}{q_3/D} \\ CONV_z &= -\frac{\frac{\partial \overline{w' \theta'}}{\partial z}}{q_3/D} \end{aligned}$$

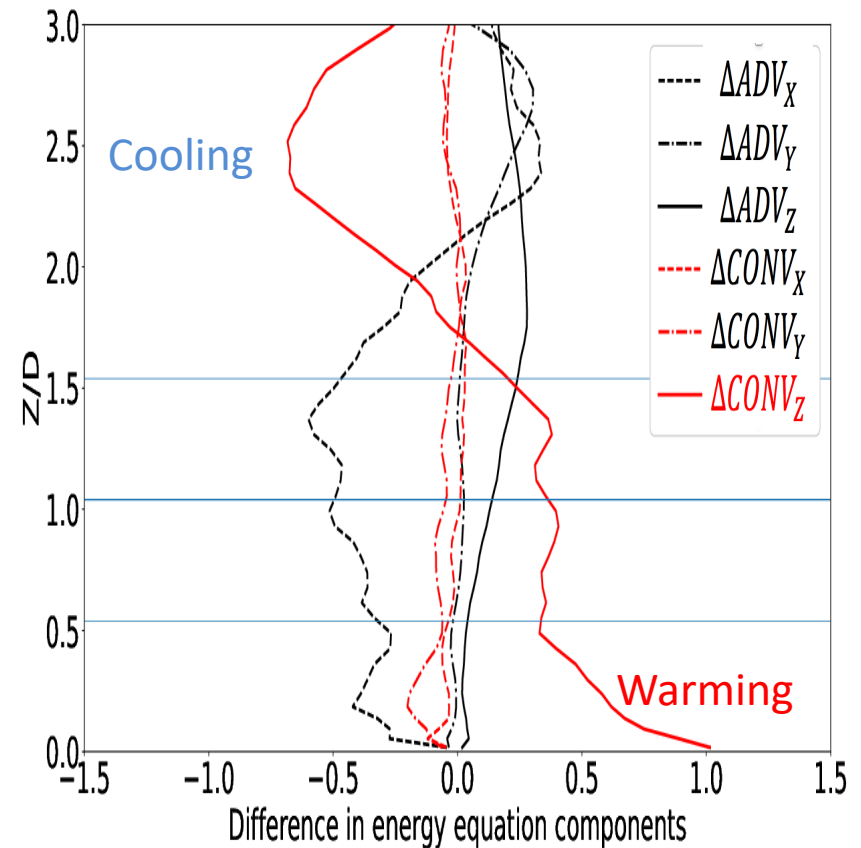


# Convergence profiles - Stable

## ONE-TURB

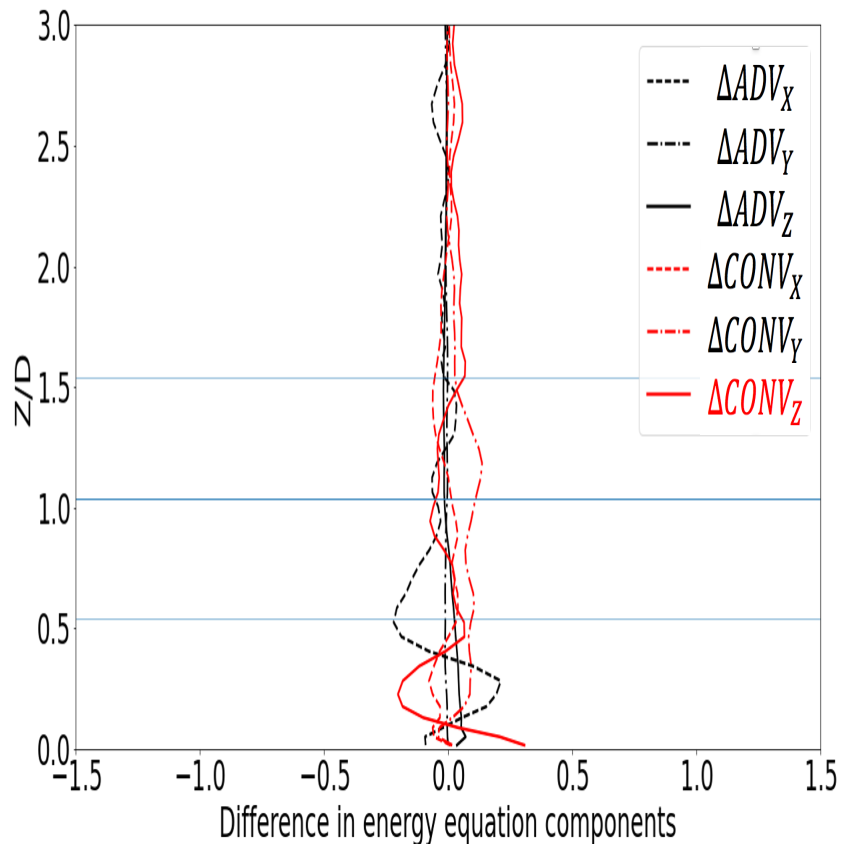


## ROW

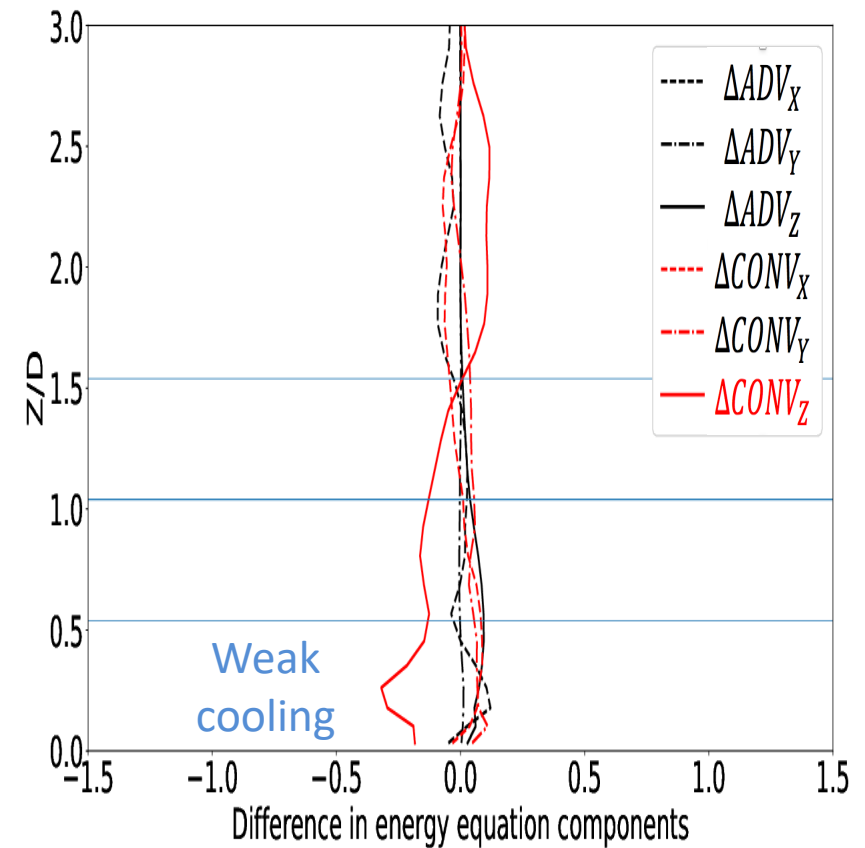


# Convergence profiles - Unstable

## ONE-TURB

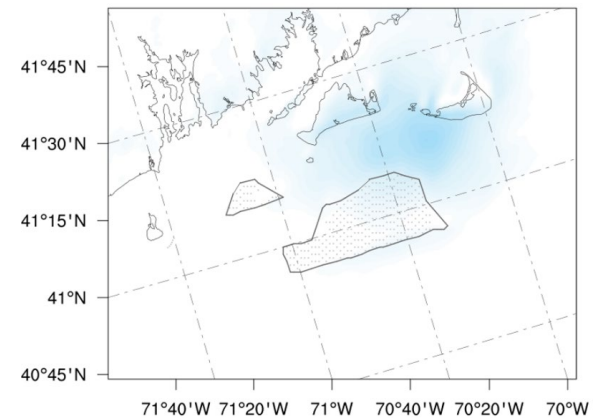
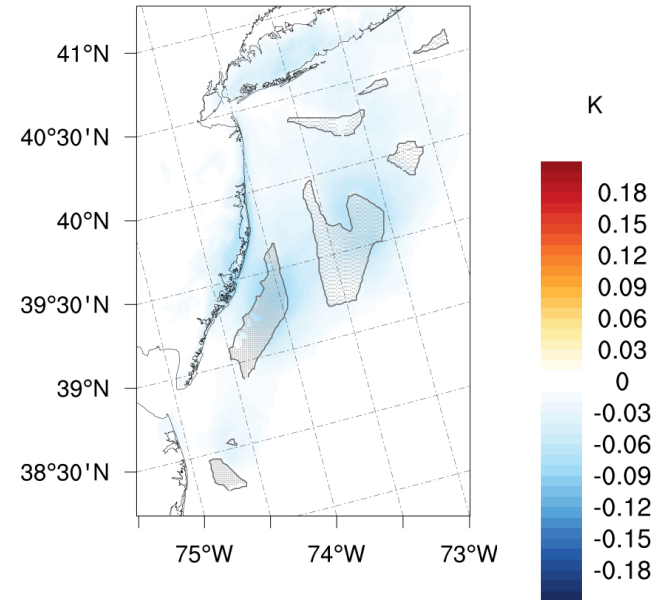


## ROW



# Surface temperature changes

## At the surface

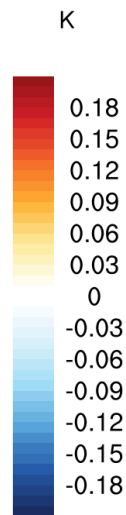
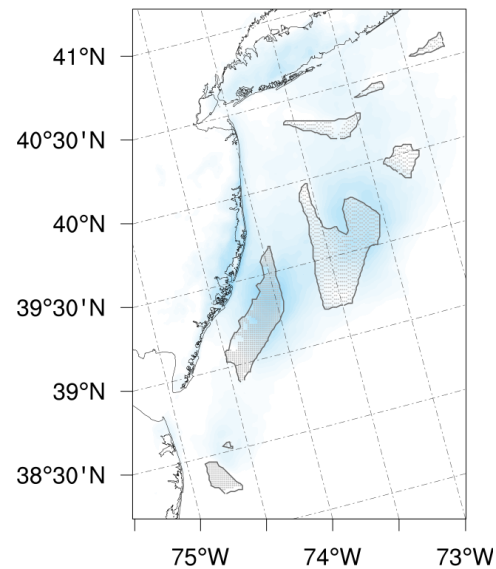
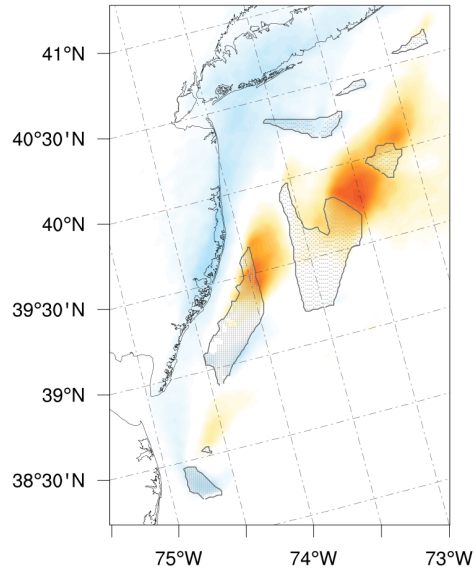
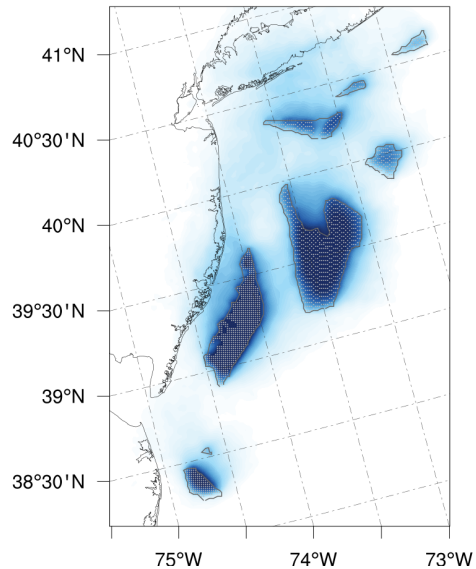


# Surface temperature changes

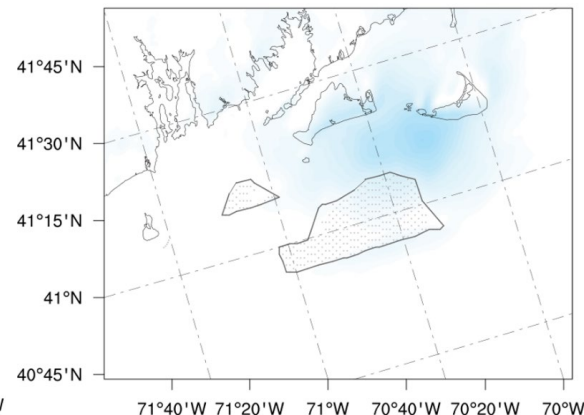
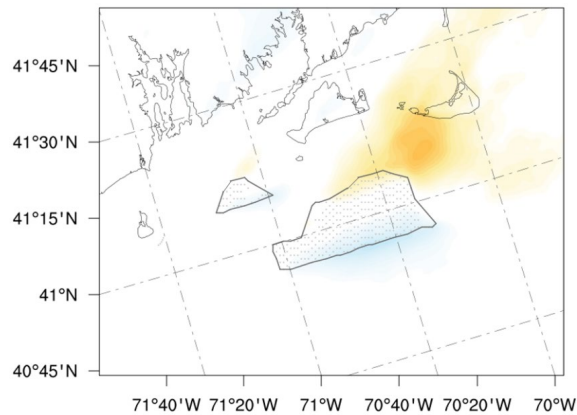
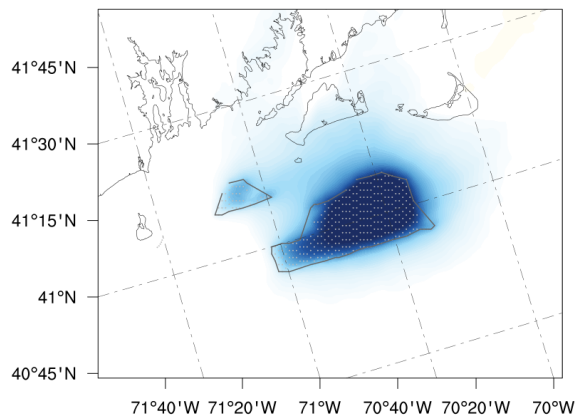
## Above hub height

## Below rotor

## At the surface

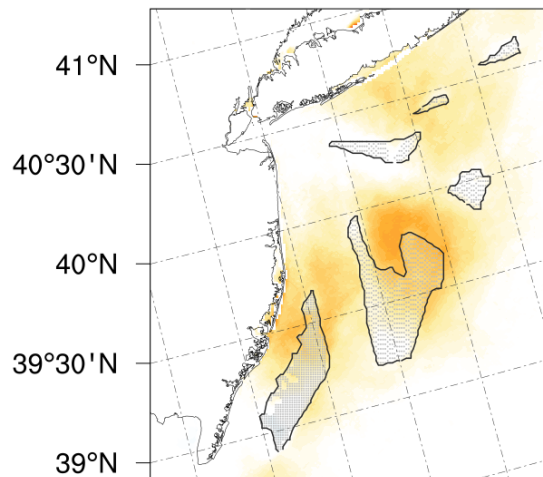


Golbazi et al., ERL 2022

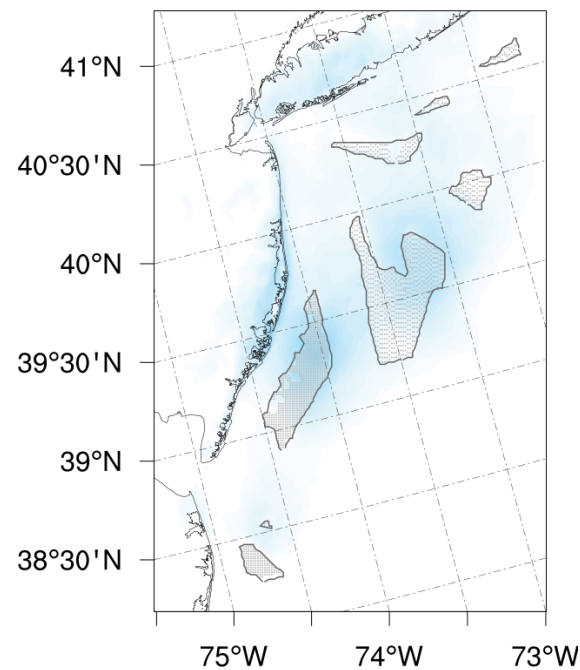




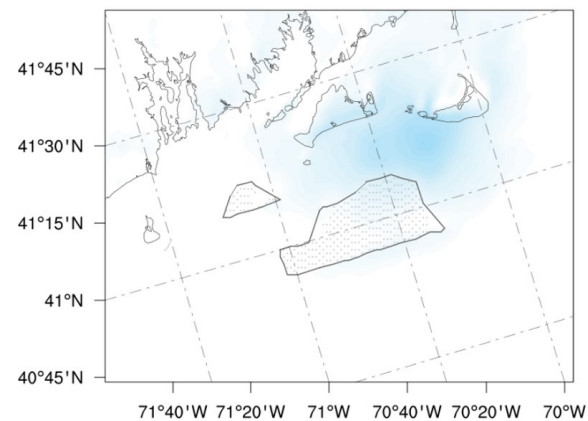
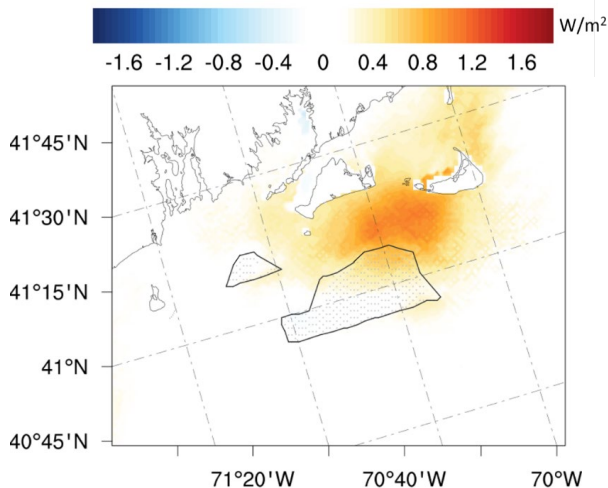
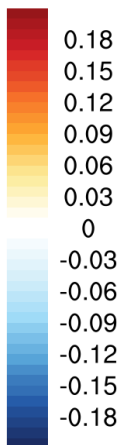
# Heat flux and temperature changes



Positive change =  
Reduction in magnitude  
of downward (negative) flux

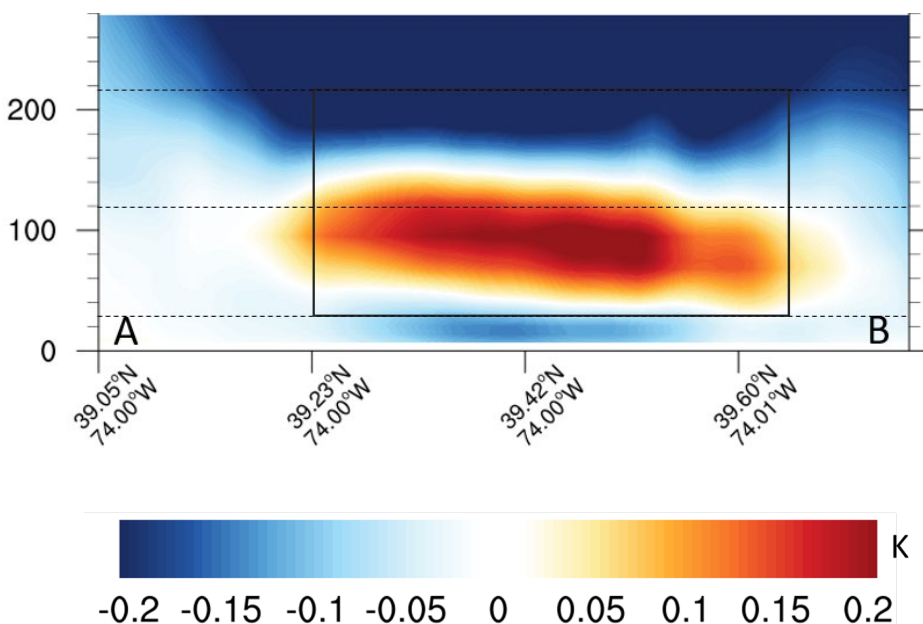


K

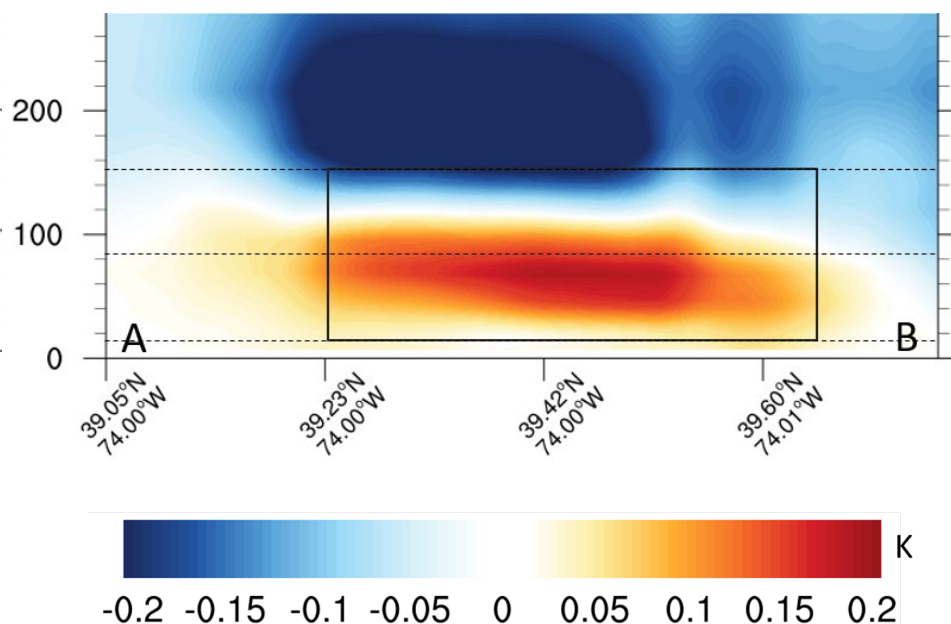


# Extreme-size turbines are tall!

**Extreme-size turbines (H = 120 m)**



**Conventional turbines (H = 80 m)**

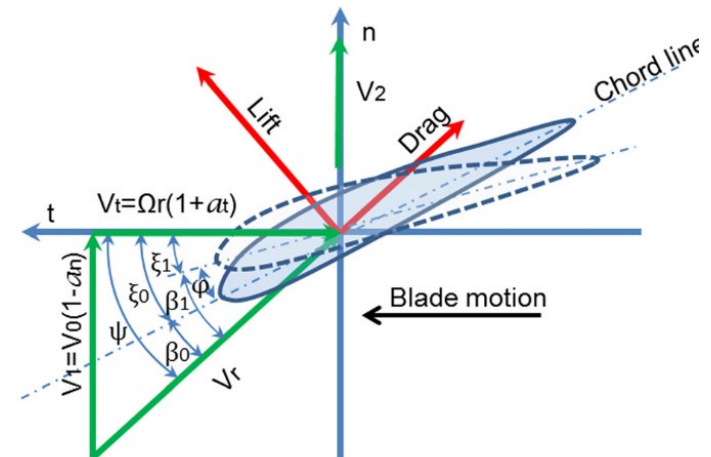
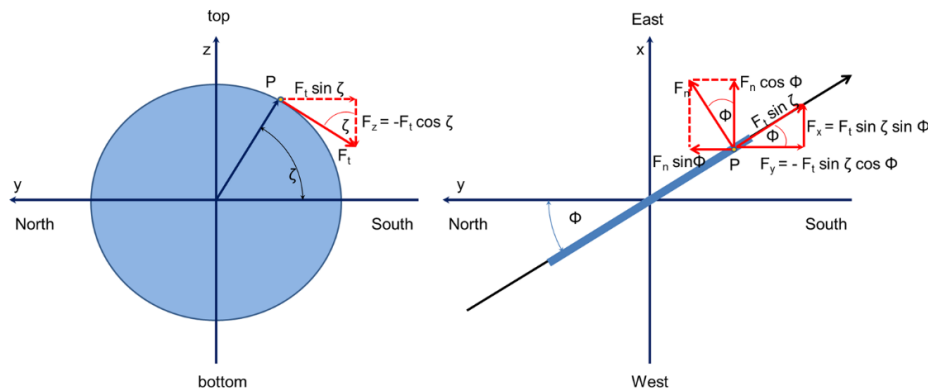


# Conclusions

- Wake effects at the ground that occur ~always:
  - Reduced wind speed;
  - Reduced turbulence;
  - Reduced heat fluxes.
- Surface temperature effects depend on:
  - Boundary layer stability (must include rotor);
  - Divergence of heat fluxes;
  - Turbine hub height.

# WRF-LES

- **Part of the Weather Research and Forecasting (WRF) model**
  - Widely used weather forecasting model
  - Full compressible Navier-Stokes equation using finite differencing
- **Wind turbine modeled as a Generalized Actuator Disk (Mirocha et al. 2014)**





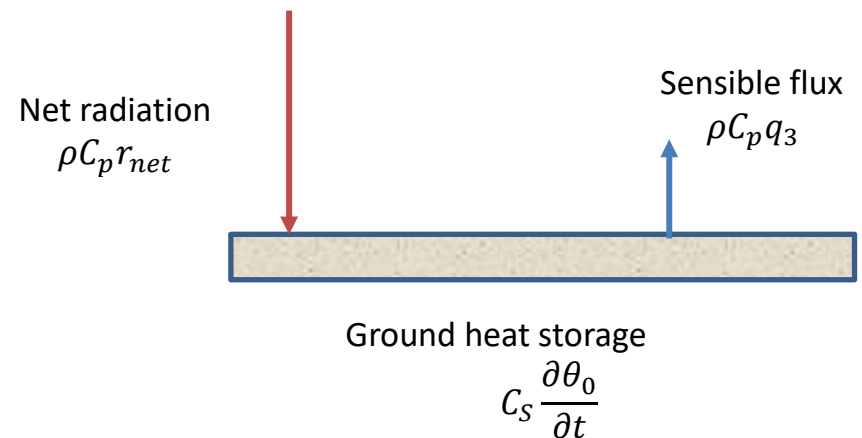
# Simplified land-surface model

## Bottom temperature: single layer slab surface model

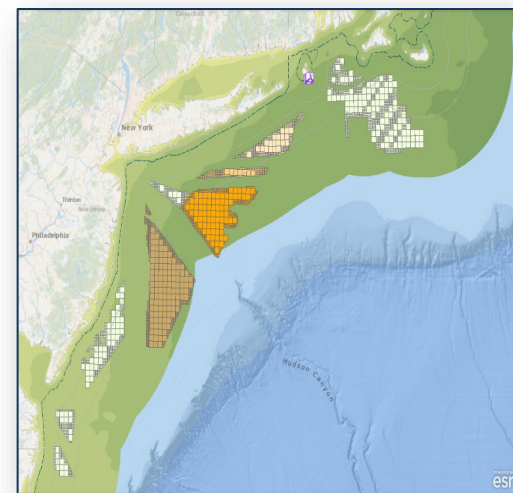
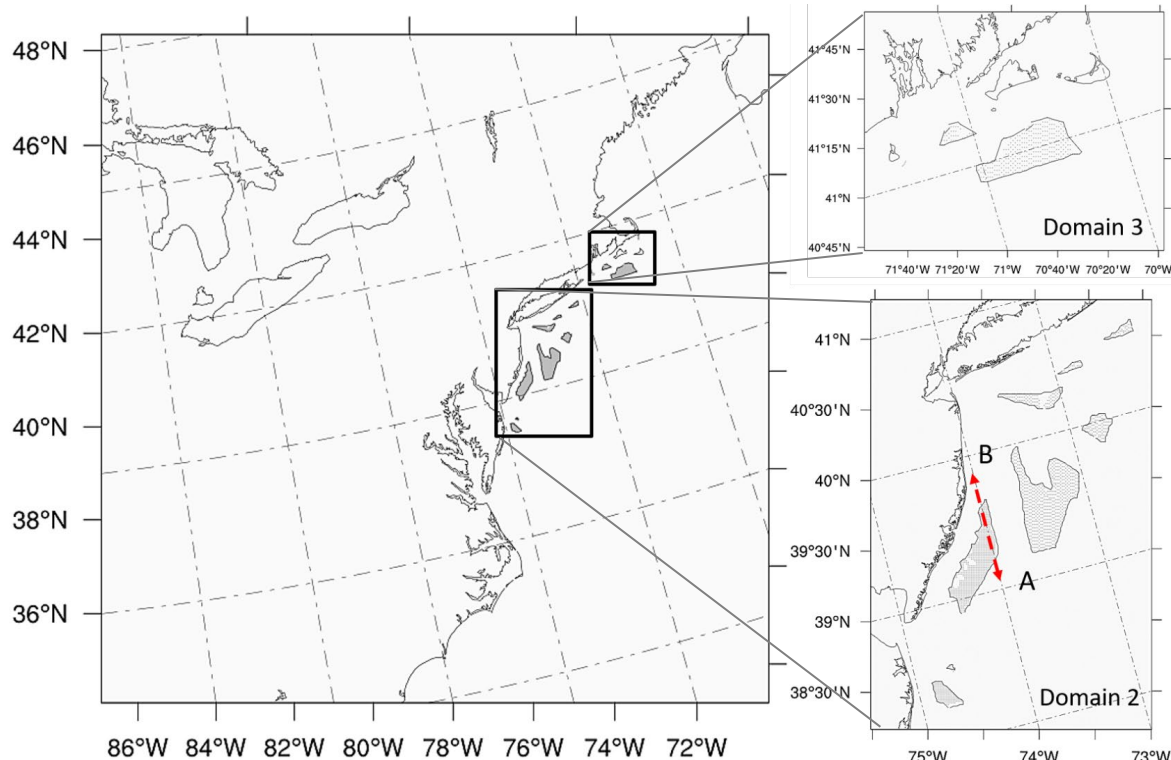
$$C_S \frac{\partial \theta_0}{\partial t} + \rho C_p (r_{net} - q_3) = 0$$

- $C_S$  Equivalent soil heat capacity per unit area, estimated from VERTEX field campaign data ( $1.6 \times 10^6 J K^{-1} m^{-2}$ )
- $\theta_0$  Ground temperature
- $\rho C_p$  Heat capacity of air
- $r_{net}$  Constant net radiation

$$q_3 = \frac{u_* \kappa (\theta_{SK} - \tilde{\theta})}{\ln(\frac{Z}{Z_0}) - \Psi_H}$$



# 30 GW of offshore wind by 2030

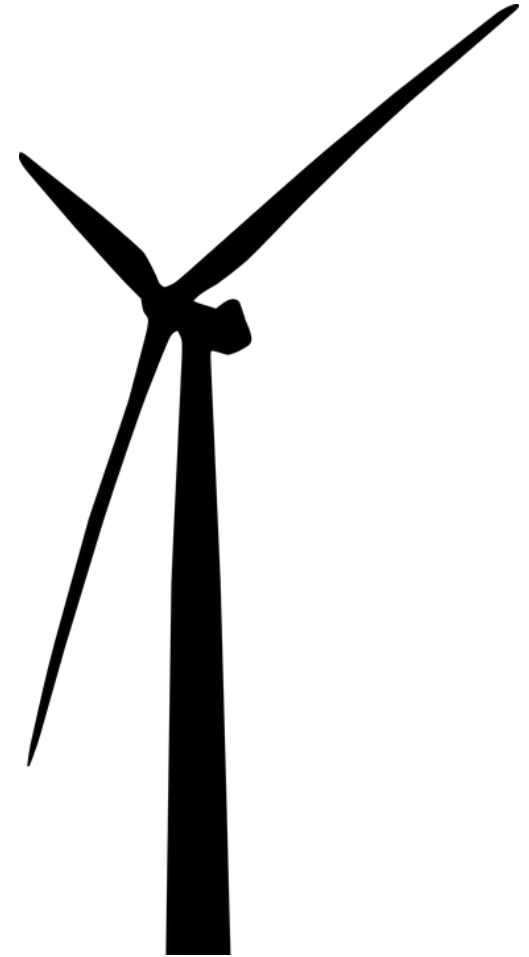


## WRF simulations with Fitch

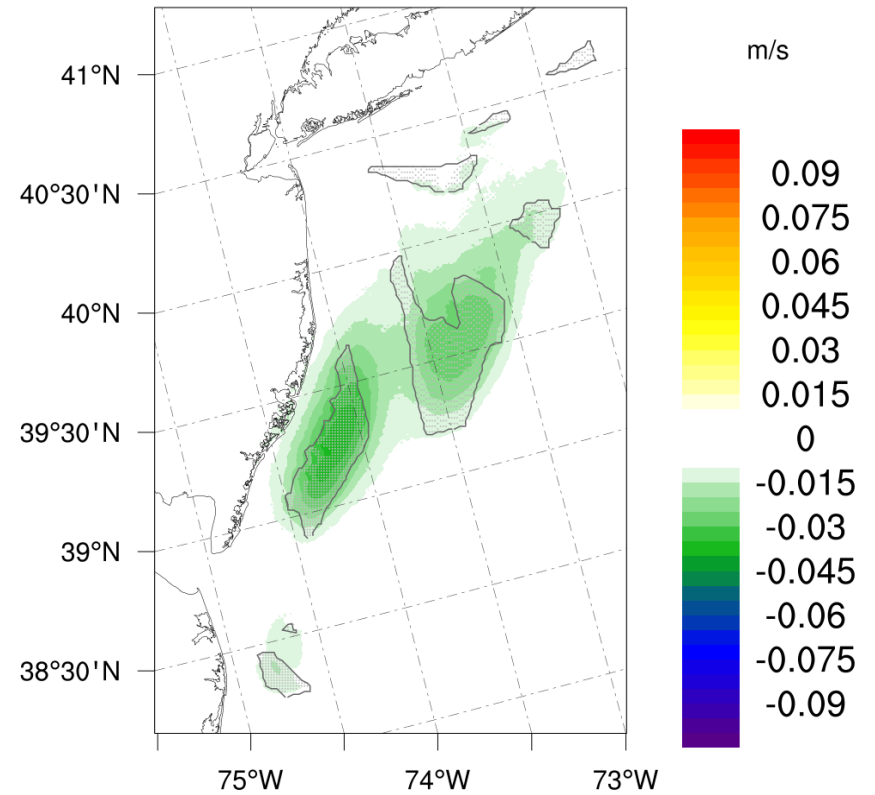
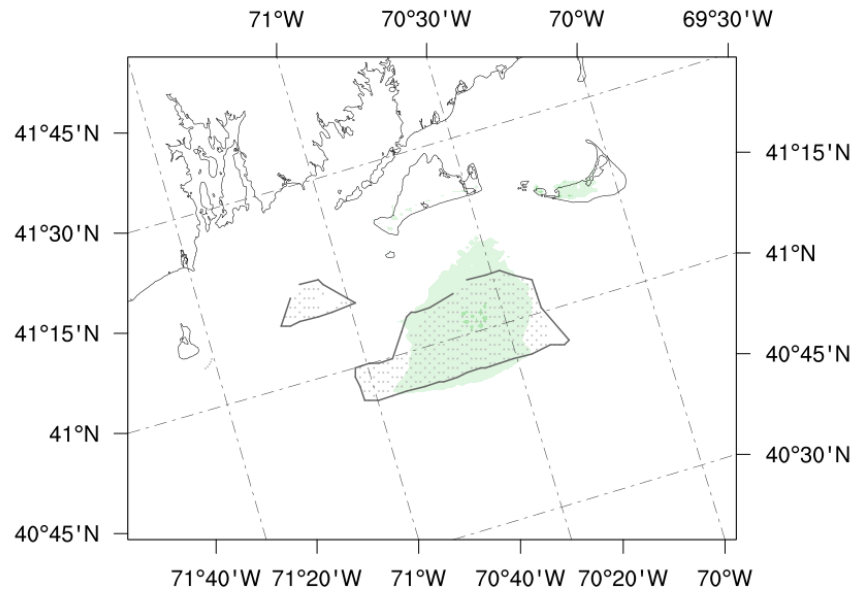
Domain	Characteristics	
Parent Domain	400 x 400	4 km
Domain 2: NJ & NY & MD & DE	260 x 170	1.3 km
Domain 3: MA, RI, CT	132 x 105	1.3 km

# Extreme-size wind turbines

Parameter	Value
Rating	10 MW
Rotor diameter	178.3 m
Hub height	119 m
Cut-in, Rated, Cut-out wind speeds	4 m/s, 11.4 m/s, 25 m/s

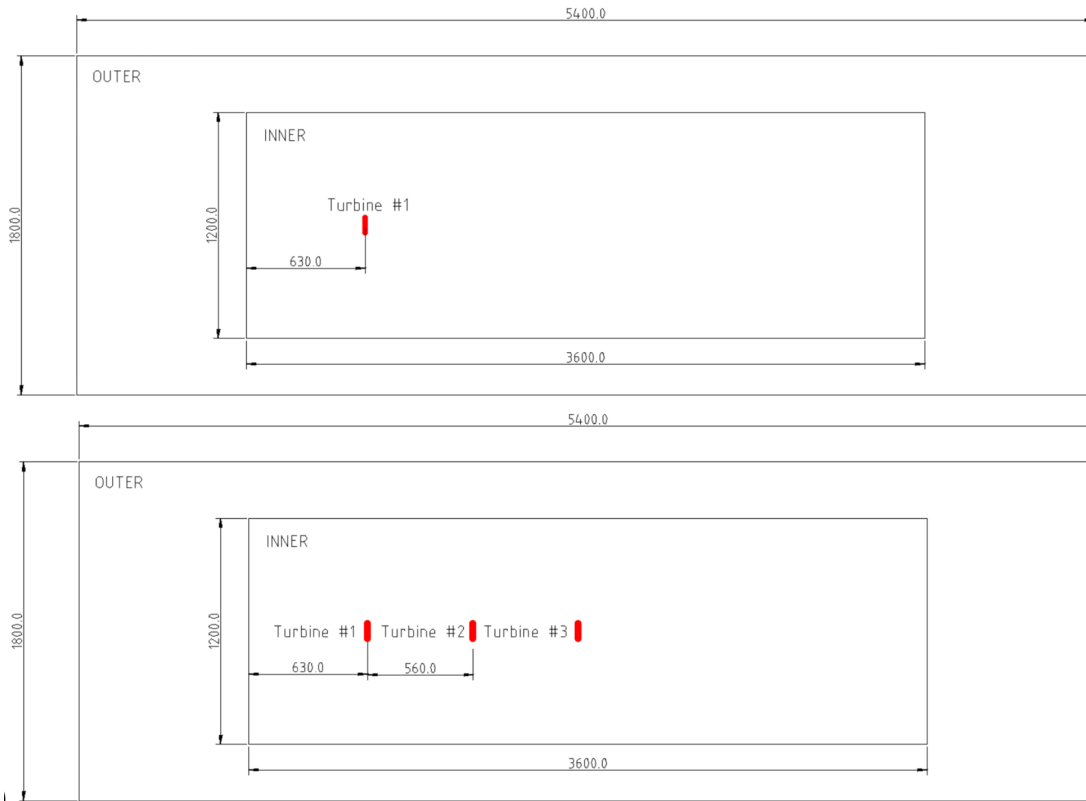


## Friction velocity



Wind speed is decreased at the surface. It influences the surface friction and decreases the friction velocity.

# WRF-LES setup



- Turbine (actuator model):
  - PSU 1.5 MW;
  - Hub 80 m;
  - Diameter 77 m.
- One-way nested domain
  - Outer domain: 5400 m x 1800 m (@15 m, periodic);
  - Inner domain: 3600 m x 1200 m (@5 m, nested).
- Domain height depends on stability.
- Three configurations, three stabilities each:
  - **NO-TURB** (no turbines);
  - **ONE-TURB** (one turbine);
  - **ROW** (three turbines).



# Profiles without turbines (NO-TURB)

